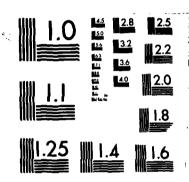
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CONNECTICUT RIVER BASIN CANAAN, NEW HAMPSHIRE

# GOOSE POND DAM NH 00118

NHWRB 36.01

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM





DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

MAY 1979

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#### DEPARTMENT OF THE ARMY

## NEW ENGLAND DIVISION, CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM, MASSACHUSETTS 02154

REPLY TO ATTENTION OF: NEDED

JUN 2 9 1979

Honorable Hugh J. Gallen Governor of the State of New Hampshire State House Concord, New Hampshire 03301

Dear Governor Gallen:

I am forwarding to you a copy of the Goose Pond Dam Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Water Resources Board, the cooperating agency for the State of New Hampshire. In addition, a copy of the report has also been furnished the owner, the State of New Hampshire, New Hampshire Water Resources Board, Concord, New Hampshire 03301, ATTN: Mr. George M. McGee, Sr., Chairman.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Water Resources Board for your cooperation in carrying out this program.

Sincerely yours,

Incl As stated JOHN P. CHANDLER Colonel, Corps of Engineers

Division Engineer

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Connecticut River Basin Canaan, New Hampshire Goose pond Dam

20. ABSTRACT (Continue on reverse side if necessary and identify by block masher)

The dam is a 1240 ft. long earthfill dam. The maximum height of the dam is 31 ft. The dam is judged to be in fair condition. It is intermediate in size with a high hazard potential classification. The slope on the upstream slope east of the spillway should be re-established. The exposed concrete surface of the core wall should be repaired.

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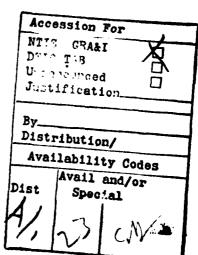
GOOSE POND DAM

NH 00118

NHWRB 36.01



CONNECTICUT RIVER BASIN CANAAN, NEW HAMPSHIRE



PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

#### NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

Identification No.: NH 00118

Name of Dam: Goose Pond Dam

Town: Canaan

County & State: Grafton, New Hampshire

Stream: Goose Pond Dam
Date of Inspection: June 8, 1978

#### BRIEF ASSESSMENT

Goose Pond Dam is located in the central western part of the State of New Hampshire, approximately nine miles northeast of the City of Lebanon. It is a 1,240-foot long earth fill dam that was reconstructed in 1952, with an upstream concrete core wall and riprap on the upstream face. The maximum height of the dam is 31 feet. The concrete spillway is an Ambursen box type modified for flood discharge. It has an effective length of 50 feet and is topped with sectional flashboards.

Based on visual inspection, available records and past operational performance, the dam is judged to be in fair condition. Standing water was noted at the toe of the eastern and western embankments. Riprap on the upstream slope eastern of the spillway and for a length of 40 feet has been partially washed away. Erosion of the concrete core wall was also noted. Continuance of this classification depends on proper operations and maintenance of the dam.

This dam falls under the category of high hazard potential, and it is intermediate in size. The test flood peak inflow is equal to the probable maximum flood, 28,730 cfs, and the test flood peak outflow is 3,650 cfs obtained as a result of routing the test flood through the pond. Hydraulic analysis indicates that the maximum surcharge pool elevation will be 105.3 (local datum) approximately 7 feet below the top of the dam. The project will pass the test flood peak outflow without overtopping the dam, and therefore, the spillway capacity is adequate.

The following recommended operation and maintenance measures, as stated in Section 7.3, be implemented within 1 year of the receipt of this Phase I report by the owner:

- The slope protection on the upstream slope east of the spillway should be re-established.
- The exposed concrete surface of the core wall should be repaired.

- 3. The areas where standing water was observed should be monitored regularly to determine the cause and then corrective measures should be taken.
- 4. Vegetation should be removed except for grass cover that prevents slope erosion.
- 5. Upstream slope of the dam and the intake structure should be inspected at low water.
- 6. A program of regular maintenance should be established.
- 7. A program of technical annual periodic inspection of the project features should be prepared and initiated.
- 8. A plan for surveillance and a warning system should be developed for periods of unusually heavy rains and runoff.

FAY, SPOFFORD & THORNDIKE, INC. By

JURGIS
GIMBUTAS
6131

OLETER

STORESSIONAL ENGINEER

Jurgis Gimbutas, P.E. Project Engineer

Richard W. Albrecht, P.E. Vice President

This Phase I Inspection Report on Goose Pond Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the Recommended Guidelines for Safety Inspection of Dams, and with good engineering judgment and practice, and is hereby submitted for approval.

Charles G. Tiersch

CHARLES G. TIERSCH, Chairman Chief, Foundation and Materials Branch Engineering Division

FRED J. RAVENS, Jr., Member

Chief, Design Branch Engineering Division

SAUL COOPER, Member Chief, Water Control Branch Engineering Division

APPROVAL RECOMMENDED:

JOE B. FRYAR

Chief, Engineering Division

B. Fregar

#### **PREFACE**

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonable possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition, and the downstream damage potential.

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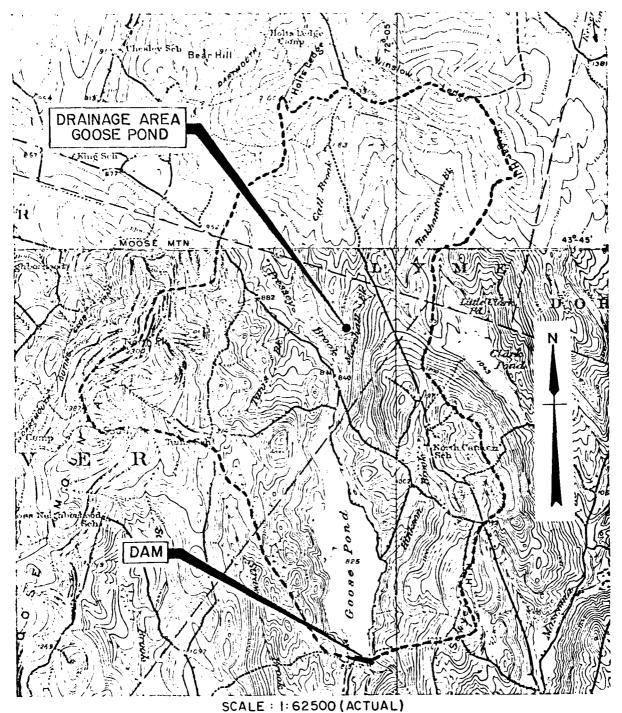
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GOOSE POND DAM, LOOKING WEST Negative No. 8-1A



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UNITED STATES
DEPARTMENT OF INTERIOR
GEOLOGICAL SURVEY

NEW HAMPSHIRE-VERMONT MASCOMA QUADRANGLE 1927 MT. CUBE QUADRANGLE 1931

#### GOOSE POND DAM

#### SECTION 1 - PROJECT INFORMATION

#### 1.1 General

#### a. Authority

Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Fay, Spofford & Thorndike, Inc., Engineers, have been retained by the New England Divison to inspect and report on selected dams in the State of New Hampshire. Authorization and notice to proceed was issued to Fay, Spofford & Thorndike, Inc., under a letter of May 3, 1978, from Mr. Ralph T. Garver, Colonel, Corps of Engineers. Contract No. DACW 33-78-C-0308 has been assigned by the Corps of Engineers for this work.

#### b. Purpose

- (1) Perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) Encourage and prepare the states to initiate quickly effective dam safety programs for non-Federal dams.
- (3) To update, verify, and complete the National Inventory of Dams.

#### 1.2 Description of Project

#### a. Location

Goose Pond is located in the central western part of the state of New Hampshire. The dam is located on the southern tip of the pond, within the Town of Canaan, and nine miles northeast of Lebanon. The outlet, Goose Pond Brook, is a tributary to the Mascoma and Connecticut Rivers. There is a road and about twenty houses located along the eastern shores of Goose Pond and several houses are located near the dam on the downstream side. The nearest town is Enfield,

which is about 7 miles downstream and along the courses of Goose Pond Brook and Mascoma River.

#### b. Description of Dam

This is a rolled earth dam with a concrete core wall. The overall dimensions are 1,240 feet in length, 31 feet in height, and 12 feet wide at the top. The earth embankment has an upstream slope of 1 vertical to 2 1/2 horizontal, covered with riprap (Photographs No. 1 and 11, Appendix C) and a downstream slope of 1 vertical to 2 horizontal. There are four clean-out basins along the downstream toe near the east end of the dam (Photograph No. 13, Appendix C).

The concrete spillway is of rectangular Ambursen type, 15 feet wide, with flashboards on three sides, for a total effective length of 50 feet (Photographs No. 2 and 3, Appendix C). At the bottom of the intake structure, there is a rectangular concrete culvert, 10 feet wide by 10 feet high with stop logs at the upstream end (Photograph No. 4, Appendix C). There are two 4-foot by 4-foot gates with the sill 29.5 feet below the top of the dam. The gates discharge into the same culvert. The manually-operated gate shafts are supported on a platform over the spillway. This platform has concrete piers, steel beams, and a creosoted planking floor (Photograph No. 14, Appendix C).

The discharge sluiceway on top of the culvert is 11 feet wide and is located near the center of the dam. It is wider on the downstream side and has concrete wingwalls. The culvert, projecting approximately 50 feet downstream, serves as an apron for the spillway overflow (Photographs No. 6, 7, and 8, Appendix C). There is a footbridge across the sluiceway, connecting both halves of the embankment.

#### c. Size Classification

The storage capacity at the spillway crest is 11,688 acre-feet, which falls in the range  $\geqslant 1,000$  and < 50,000 acre-feet. On the basis of Table 1, Size Classification, in the "Recommended Guidelines for Safety Inspection of Dams," furnished by the Corps of Engineers, the dam is classified as intermediate in size.

#### d. Hazard Classification

In the event of failure of this dam, the town of Enfield, which is at a distance of approximately 7 miles downstream of the dam, will be in danger of being flooded. The depth of the water at the damage impact area, as shown on page 14 in Appendix D, is estimated. It is also estimated that in the event of failure of this dam, loss of more than a few lives and excessive property damage would probably

occur. Therefore, on the basis of Table 2, Hazard Potential Classification, in the "Recommended Guidelines for Safety Inspection of Dams," furnished by the Corps of Engineers, this dam falls in the category of high hazard potential.

#### e. Ownership

During construction of this dam between 1917 and 1918, the owner was the Mascoma River Improvement Company of Lebanon, New Hampshire. In 1936, the same owner was referred to as a subsidiary of the New England Power Service Company.

In 1938, the owner was the Granite State Electric Co. of Lebanon, New Hampshire, which was also affiliated with the New England Power Service Company. Since 1969, Goose Pond Dam, the water rights and land connected therewith were acquired by the New Hampshire Water Resources Board. Therefore, the present owner is the State of New Hampshire.

#### f. Operator

The dam is being operated by the New Hampshire Water Resources Board, 37 Pleasant Street, Concord, New Hampshire, telephone (603) 271-3406. Mr. Vernon Knowlton is the chief engineer.

#### g. Purpose of Dam

Goose Pond Dam was built to store spring run-off waters in order to maintain normal flow needed for power plants on Mascoma River. While doing this, the dam helps to maintain the required water level for recreation. There are numerous cottages and houses on the lake shore.

#### h. Design and Construction History

The original dam was a rock filled timber crib dam built in the 19th century and approximately 10 feet high. It had a 59-foot long spillway and a trap gate at the base of the dam to drain the pond. It was impractical to repair this dam, and a new earth embankment with a concrete core wall was constructed between August, 1917, and July, 1918. The new dam was designed by Mascoma River Improvement Company, Engineering Department, Turners Falls, Massachusetts. The contractor was H. P. Cummings Construction Co., Canaan, New Hamphire. The new dam was constructed about 50 feet downstream from the old dam. The earth embankment required 19,000 cubic yards of material and the core wall 1,450 cubic yards of concrete. The new dam is approximately 12 feet higher than the existing one. A rectangular Ambursen

type reinforced concrete spillway with concrete cut-off walls, bulk-head walls, an apron, and a sluiceway constituted the intake/discharge structure. It is located near the center of the 1240-foot long dam.

During construction of the dam in the winter of 1917-1918, Mr. Arthur T. Safford, a consulting engineer of Lowell, Massachusetts, was consulted regarding the safety of the unfinished dam to pass the oncoming spring freshet.

The owner undertook major repairs and improvements of the dam in 1952. It was engineered by the New England Power Service Company, Boston, Massachusetts. The New Hampshire Water Resources Board approved the owner's petition for reconstruction on June 16, 1952. The work was done between October, and December, 1952. The spillway discharge was increased by reducing the elevation of the concrete crest by 5 feet and installing 5-foot flashboards. A stop log section was constructed, and the discharge conduit was covered to make a rectangular culvert. The top width of the earth dike was increased from 5 feet to 12 feet and was regraded. The concrete core wall was strengthened by widening the footings and adding concrete buttresses.

#### i. Normal Operational Procedure

This dam is checked weekly by personnel of the New Hampshire Water Resources Board using their established procedures. The only control available to lower the pond level is a 10-foot by 10-foot concrete conduit that is regulated by two gates and stop logs, both of which are manually operated.

#### 1.3 Pertinent Data

All the elevations and information presented below are with respect to local datum. According to the U.S.G.S. Quadrangle Sheet, the top of the spillway flashboard, Elevation 106.5 (local datum), is equal to 825 msl (estimated).

#### a. Drainage Area

Goose Pond as shown on the U.S.G.S. Quadrangle Sheet is located on the headwaters of Goose Pond Brook. It has a total drainage area of 15.7 square miles and the watershed is highly wooded and mountainous.

#### b. Discharge at Dam Site

Outlet works (sluice culvert) - size 10 feet by 10 feet at Invert Elevation 83.0 (Photograph No. 4, Appendix C). The estimated discharge capacities of this culvert

are given below with both gates, each 4 feet by 4 feet, fully open and stop logs closed:

608 cfs at Reservoir Elevation 101.5 (top of concrete spillway)

704 cfs at Reservoir Elevation 106.5 (top of flash-boards)

- (2) Maximum known flood at dam site information not available.
- (3) Ungated spillway capacity at top of dam 6700 cfs at Elevation 112.50.
- (4) Ungated spillway capacity at test flood maximum pool elevation - 3650 cfs at Elevation 105.3 (see page 13 in Appendix D).
- c. Elevation (Feet above local datum)
  - (1) Top of dam 112.5.
  - (2) Test flood maximum pool 105.3.
  - (3) Top of flashboards 106.5.
  - (4) Spillway crest (top of concrete) 101.5.
  - (5) Stream bed at centerline of dam 81.5.
  - (6) Maximum tailwater 86.0 (estimated).
- d. Reservoir
  - (1) Length of maximum pool 3.2 miles (estimated).
  - (2) Length of recreation pool 2.5 miles.
  - (3) Length of flood control pool not applicable.
- e. Storage (Acre-Feet)
  - (1) Top of dam 15,800 acre-feet.
  - (2) Test flood maximum pool elevation 10,800 cfs.

- (3) Recreation pool unknown.
- (4) Spillway crest 8,487 acre-feet.

#### f. Reservoir Surface (Acres)

- (1) Top of dam 740 acres (estimated).
- (2) Maximum pool 650 acres (estimated).
- (3) Flood control pool not applicable.
- (4) Recreation pool unknown.
- (5) Spillway crest 610 acres.

#### g. Dam

- (1) Type Earth fill embankment.
- (2) Length 1,240 feet.
- (3) Height 31 feet.
- (4) Top width 12 feet.
- (5) Side slopes
  - (a) Upstream Approximately 1 vertical to 2.5 horizontal.
  - (b) Downstream l vertical to 2 horizontal.
- (6) Zoning Not applicable.
- (7) Impervious core Not applicable.
- (8) Cutoff Upstream concrete core wall.

#### h. Spillway

- (1) Type Rectangular (Ambursen).
- (2) Length of weir Effective length 50 feet.

	(3)	Crest elevation (top of concrete)	
		(a) Front	104.5.
		(b) Sides	101.5.
	(4)	Flashboard	Pin-type flashboards - 5 feet and 2 feet high.
		(a) Crest elevation (top of board)	106.5.
	(5)	U/S Channel	Pond.
i.	Regu	lating Outlets	
	(1)	Invert	88.5 upstream and 81.3 downstream.
	(2)	Size	10-foot by 10-foot sub- merged culvert with a 10-foot by 15-foot en- trance opening.
	(3)	Description	Rectangular concrete cul- vert.
	(4)	Control mechanism	Stop logs and two 4-foot by 4-foot gates, manually operated.

#### SECTION 2 - ENGINEERING DATA

#### 2.1 Design

Drawings indicating plans, elevations and sections of the dam and appurtenant structures, including the details of the discharge facilities, are available from project records. Selected drawings are included in Appendix B, following the listing of records, and past inspection reports. Soil Profiles, limited in nature, are also available from project records.

#### 2.2 Construction

No engineering data are available on the construction of this dam.

#### 2.3 Operation

No engineering operational data was disclosed. The original use of the storage in this pond was for generation of hydropower. Presently, the pond is used for recreation. Goose Pond is a part of the Mascoma River storage system. The operation of Goose Pond is interlinked with the operation of the remaining three lakes of the Mascoma River system, namely, Grafton Pond, Crystal Lake, and Mascoma Lake. Goose Pond is the largest of four ponds in the terms of storage volume. The pond is filled by spring runoff, and the resulting stored water is gradually released during the summer to supplement dry weather flow in the Mascoma River and to maintain the level of Mascoma Lake. The fall rains result in additional water being stored for use during the winter months and to keep the channel open at the Lebanon water Works Pumping Station. The pond level is dropped to a point consistent with the amount of snow cover to make room for spring runoff.

#### 2.4 Evaluation

#### a. Availability

Pertinent structural, geotechnical, and hydrologic data, which formed the basis of the design of the dam, are available on a limited basis.

#### b. Adequacy

Sufficient engineering data are available for a Phase I inspection.

#### c. Validity

The available data is considered valid on the basis of the results of the visual inspection.

#### SECTION 3 - VISUAL INSPECTION

#### 3.1 Findings

The Phase I inspection of the Goose Pond Dam was performed on June 8, 1978. A copy of the inspection check list is included in Appendix A.

#### a. General

In general, the soil features are in fair condition. The concrete was observed to be in poor to good condition, see subparagraph c.

#### b. Dam

No evidence of vertical or horizontal misalignments was observed. There is no indication of sloughing, bulging, or movement of the slopes nor is there any evidence of piping.

The riprap slope protection on the upstream slope is in poor to fair condition. A section of the slope protection, approximately between 66 feet and 105 feet east of the spillway, has been washed away.

Standing water, approximately 300 feet west of the spillway, was observed at the toe of the western embankment. The area appears inadequately graded for drainage, and it is probable that the water observed is a combination of runoff and seepage.

At the toe of the eastern embankment between the two extreme eastern clean-out basins, standing water was observed. The area downstream of the dam in this area is not adequately graded for drainage, and it is probable that this water is trapped runoff rather than seepage.

The four clean-out basins located east of the spillway are in good operating condition. Visual observations indicate approximately 2 to 4 inches of sand in the bottom of the basin.

Vegetation, consisting of grass and weeds, was noted on the upstream slopes and on the top of the dam. Small bushes were observed on the downstream slope.

#### c. Appurtenant Structures

At the time of our inspection, the water level of the pond was at elevation 106.6 (local datum), approximately 0.1 foot above the top of the spillway flashboard. Therefore, we could not visually inspect the intake structure, the outlet culvert (10 feet by 10 feet), the two 4-foot by 4-foot gates regulating flow into the outlet culvert due to the fact that they were underwater.

The concrete of the spillway and its wingwalls above the water level was observed to be in good condition. Joint alignment is generally good and no erosion was noted.

The manually operated gate shafts are supported on a platform over the spillway. The cresoted wooden planking floor of the platform and the footbridge is in very good condition. The flashboards and the manually operated gate shafts were observed to be in operable condition. The railings of the platform and the footbridge are in good condition.

The exposed concrete of the core wall is in poor condition. Both horizontal and vertical cracks were observed with numerous areas of erosion. The concrete of the outlet structure and its wingwalls above the water level was observed to be sound. Joint alignment is generally good and no erosion was noted.

#### d. Reservoir Area

Goose Pond covers 668 acres in the towns of Canaan and Hanover in Grafton County, New Hampshire. It was formed by a dam on the Goose Pond Brook, which is a tributary to the Mascoma River, and is located 8.6 miles above Mascoma Dam. The pond collects the runoff from a drainage area of 15.7 square miles. The pond is approximately 2.5 miles long. There are several private cottages and year-round residences located on the shores of the pond. The reservoir shores are heavily wooded.

#### e. Downstream Channel

The downstream channel and side slopes are in good condition.

#### 3.2 Evaluation

The observed condition of the dam is fair. The potential problems observed during the visual inspection are listed as follows:

a. Standing water at the toe of the eastern and western  $\mbox{\sc embank-ments.}$ 

- b. Erosion of the exposed concrete of the core wall.
- c. Lack of slope protection on the upstream slope between 66 feet and 105 feet east of the spillway.

#### SECTION 4 - OPERATIONAL PROCEDURES

#### 4.1 Procedure

The New Hampshire Water Resources Board has operated Goose Pond Dam since 1969. The Pond level is maintained by a box type spillway located at the center of the dam. The flow is controlled by sectional flashboards 5 feet high and 2 feet high. The only control available to lower the pond level is a 10-foot by 10-foot conduit that is regulated by two gates and stop logs, both of which are manually operated.

#### 4.2 Maintenance of Dam

The maintenance of Goose Pond Dam is the responsibility of the New Hampshire Water Resouces Board.

#### 4.3 Maintenance of Operating Facilities

Throughout the year, the Dam is visited on a weekly basis by an inspector from the New Hampshire Water Resources Board. The maintenance of the gate operating facilities controlling the flow through the undersluice at the bottom of the intake structure is satisfactory:

#### 4.4 Description of any Warning System in Effect

A flood warning system is non-existent.

#### 4.5 Evaluation

The operation and maintenance procedures for Goose Pond Dam, consisting of a weekly program of inspection, should ensure that all problems encountered can be remedied within a reasonable period of time.

#### SECTION 5 - HYDRAULIC/HYDROLOGIC

#### 5.1 Evaluation of Features

#### a. Design Data

- (1) This dam falls under the category of high hazard potential, and it is intermediate in size. Using the "Recommended Guidelines for Safety Inspection of Dams," the recommended spillway test flood peak inflow is equal to the probable maximum flood. The spillway test flood inflow hydrograph, estimated, is furnished in Appendix D. The test flood peak inflow is 28,730 cfs.
- (2) The estimated peak outflow is 3,650 cfs, corresponding to the routed spillway test flood through the pond. Refer to Appendix D for details.
- (3) The Goose Pond storage capacity versus the elevation, an estimated capacity curve, is included in Appendix D.
- (4) The estimated composite discharge rating curve for all the discharge facilities is furnished in Appendix D.
- (5) The hydrologic map of the watershed above the dam site, including the reservoir area, watercourse, and elevation contours, is furnished in Appendix D.

#### b. Experience Data

Except for limited information, past flood details are not available for this dam.

#### c. Visual Observations

The crest of the non-overflow section is l1 feet above the crest of the spillway. At the time of inspection, water was observed flowing over the flashboards on the spillway crest. The hydraulic design of the spillway is good.

#### d. Overtopping Potential

The spillway test flood peak inflow is 28,730 cfs. Using the spillway test flood inflow hydrograph, the composite rating curve for all the discharge facilities, the capacity curve, detailed flood routing computations were made, and it was found that the surcharge

elevation to be approximately 105.3 (see Appendix D for details). There is enough clearance since the top of the earth embankment is at Elevation 112.5. Therefore, the dam will not be overtopped by the test flood if all the discharge facilities are functioning at their optimum capacity.

#### SECTION 6 - STRUCTURAL STABILITY

#### 6.1 Evaluation of Structural Stability

#### a. Visual Observations

The upstream slope could not be seen due to the fact that it was under water. The visual inspection revealed the following evidence of possible stability problems:

- Standing water at the toe of the eastern and western embankments.
- (2) Lack of slope protection on the upstream slope between 66 feet and 105 feet east of the spillway.

Visual inspection of the concrete core wall and spillway section did not reveal any evidence of instability.

b. Design and Construction Data

There are no design computations available, but design drawings, dated 1917 and 1952, were obtained from project records.

c. Operating Records

Except for memorandums and correspondence listed in Appendix B, other records are not available at the office of the New Hampshire Water Resources Board.

d. Post-Construction Changes

No changes were made since 1952.

e. Seismic Stability

The dam is located in Seismic Zone 2 and in accordance with recommended Phase I guidelines does not warrant seismic analyses.

#### SECTION 7 - ASSESSMENT, RECOMMENDATIONS & REMEDIAL MEASURES

#### 7.1 Dam Assessment

#### a. Condition

Visual inspection and operational history indicates that Goose Pond Dam is in fair condition and functioning satisfactorily.

#### b. Adequacy of Information

An adequate assessment of the dam consistent with the scope of Phase I investigation has been made based upon the visual inspection and available information.

#### c. Urgency

The recommended operation and maintenance measures enumerated below should be implemented within 1 year of receipt of this Phase I report by the owner.

#### d. Need for Additional Investigation

The information available from the visual inspection is adequate to identify the potential problems which are: standing water at the toe of the western and eastern embankments, and the lack of slope protection on the upstream slope east of the spillway. These problems require the attention of the engineering staff of the New Hampshire Water Resources Board to determine the cause, and then specify remedial measures to rectify the problem. If left unattended, the problems could lead to instability of the structure.

#### 7.2 Recommendations

No major modification or engineering investigation is recommended at this time.

#### 7.3 Remedial Measures

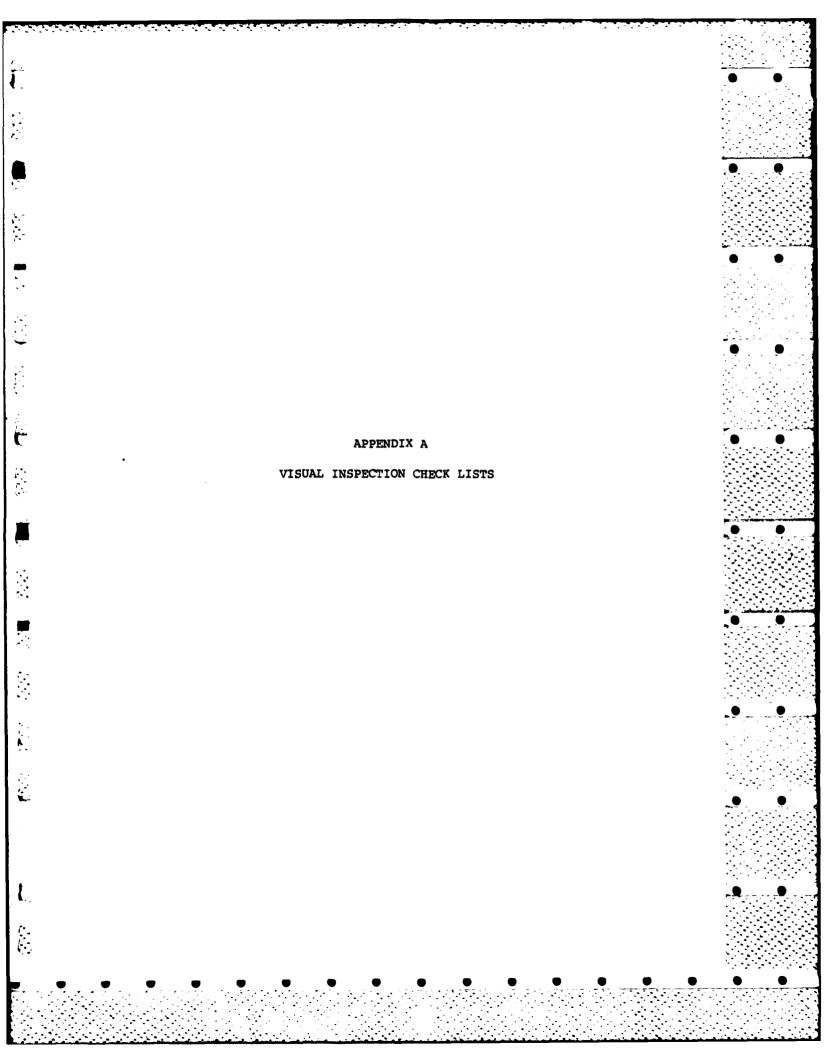
It is considered important that the following operating and maintenance procedures be attended to as early as practical:

a. The slope protection on the upstream slope between 66 feet and 105 feet east of the spillway should be reestablished. If not corrected, this could develop into a serious problem.

- b. The concrete surface of the core wall should be repaired as continued deterioration could develop into a serious problem.
- c. Standing water was observed at the toe of the eastern and western embankments. These areas should be monitored regularly to determine the cause. If it is seepage from the pond, appropriate remedial measures should be taken.
- d. Vegetation should be removed from the dam embankment, except for grass cover that prevents slope erosion.
- e. Upstream slope of dam and the intake structure should be inspected at low water.
  - f. A program of regular maintenance should be established.
- g. A program of technical annual periodic inspection of the project features should be prepared and initiated.
- h. Because the dam is located upstream of a populated area, round-the-clock surveillance should be provided during periods of high precipitation.
- i. The owner should develop a formal warning system. An operational procedure to follow in the event of an emergency should also be adopted.

#### 7.4 Alternatives

None recommended.



#### APPENDIX A

## VISUAL INSPECTION CHECK LIST PARTY ORGANIZATION

PROJECT Goose Pond Dam	DATE June 8, 1978
	TIME 1330 - 1630
	WEATHER Cloudy - Drizzle
	W.S. ELEV. 106.5 U.S. DN.S. 106.5 (local datum) = 825 ms1
PARTY:	
1. Jurgis Gimbutas, P.E.	Team Captain - Structural and Concrete
2. Harvey H. Stoller, P.E.	Soils, Geology, & Foundations
3. V. Rao Maddineni, P.E.	Hydraulics & Hydrology
PROJECT FEATURE	INSPECTED BY REMARKS
1. Dam Embankment	H. H. Stoller Fair
2. Outlet Works - Culvert	J. Gimbutas Buried
3. Outlet Structure	J. Gimbutas Good
4. Outlet Channel	H. H. Stoller V. R. Maddineni Good
5. Approach Channel	H. H. Stoller V. R. Maddineni Good
6. Spillway Weir	J. Gimbutas Good
7. Reservoir and Downstream Ch	nannel V. R. Maddineni Good

PROJECT Goose Pond Dam	DATE June 8, 1978
PROJECT FEATURE Dam Embankment	NAME Henry H Stiller
DISCIPLINE Soils & Foundations	NAME Steam I I I Come
PROJECT FEATURE	<del></del>
discipline	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
DAM EMBANKMENT	
Crest Elevation	112.5
Current Pool Elevation	106.6
Maximum Impoundment to Date	107.1
Surface Cracks	None observed
Pavement Condition	None
Movement or Settlement of Crest	None observed
Lateral Movement	None observed
Vertical Alignment	No visual vertical misalignment observed
Horizontal Alignment	No horizontal misalignment observed
Condition at Abutment and	Norma I

PROJECT Goose Pond Dam	DATE June 8, 1978
PROJECT FEATURE Dam Embankment	— - 14 M
DISCIPLINE Soils & Foundations	NAME How I It le
PROJECT FEATURE	_
DISCIPLINE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
Indications of Movement of Structural Items on Slopes	None observed
Trespassing on Slopes	None observed
Sloughing or Erosion of Slopes or Abutments	None observed
Rock Slope Protection - Riprap Failures	Poor to fair condition
Unusual Movement or Cracking at or Near Toes	None
Unusual Embankment or Downstream Seepage	See narrative (Section 3)
Piping or Boils	None observed
Foundation Drainage Features	None
Toe Drains	Good condition (clean-out basin)
Instrumentation System	None

PROJECT Goose Pond Dam	DATE June 8, 1978
PROJECT FEATURE Culvert	
DISCIPLINE Structures & Concrete	NAME - Th mist.
PROJECT FEATURE	
DISCIPLINE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
OUTLET WORKS - 10-FOOT BY 10-FOOT CULVERT	

Could not be seen

**General Condition** 

PROJECT Goose Pond Dam	DATE June 8, 1978
PROJECT FEATURE Outlet Structure	
DISCIPLINE Structures & Concrete	NAME -7:17772; TC1
PROJECT FEATURE Outlet Channel	
DISCIPLINE Soils & Foundations	NAME Planny I Itlle
DISCIPLINE Hydraulics & Hydrology	NAME 1 PRE KIUUCKENENE

AREA EVALUATED

CONDITION

OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL

Comment Condition of Comments

General Condition of Concrete Good condition

Rust or Staining None observed

Spalling None observed

Erosion or Cavitation None observed

Visible Reinforcing None observed

Any Seepage or Efflorescence None observed

Condition at Joints Good

Drain Holes None observed

Channel

Loose Rock or Trees Overhanging Channel

None observed

Condition of Discharge

Channel

Good

PROJECT Goose Pond Dam	DATE June 0, 1970
PROJECT FEATURE Spillway Weir	_
DISCIPLINE Structures & Concrete	NAME 12mmile
PROJECT FEATURE Approach Channel	- · · · · · · · · · · · · · · · · · · ·
DISCIPLINE Soils & Foundations	NAME Haven I Allin
DISCIPLINE Hydraulics & Hydrology	NAME ! PAC Aluddenen
AREA EVALUATED	CONDITION
OUTLET WORKS - SPILLWAY WEIR, APPROACH CHANNEL	
a. Approach Channel	
General Condition	Good
Loose Rock Overhanging Channel	None observed
Trees Overhanging Channel	None observed
Floor of Approach Channel	Could not be observed
b. Weir and Training Walls	

Stop logs and slots Good condition

Good

None observed

General Condition

Rust or Staining

of Concrete

Spalling

PROJECT Goose Pond Dam	DATE June 8, 1978
PROJECT FEATURE Spillway Weir	
DISCIPLINE Structures & Concret	e NAME 1 CZIMANIA
PROJECT FEATURE	<u> </u>
DISCIPLINE	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
Any Visible	
Reinforcing	None observed
Any Seepage or	
Efflorescence	None observed

APPENDIX B EXISTING AVAILABLE INFORMATION

#### APPENDIX B

#### 1. Listing of Records and Their Location

The New Hampshire Water Resources Board, 37 Pleasant Street, Concord, New Hampshire, has four folders of records and correspondence from 1915 to 1977. These folders are filed under Town/Dam No. 36.01, Canaan/Goose Pond.

The documents of importance to the design and maintenance of the dam are as follows:

- (1) June, 1917 to July, 1918. Letters regarding the design and construction of an earth dam and concrete spillway in lieu of an old worn out timber crib. The correspondence regarding the sand and gravel test results was written by representatives of the Connecticut River Conservation Co., Turners Falls, Massachusetts; the Public Service Commission, Concord, New Hampshire; and Pittsburgh Testing Laboratory, Pittsburg, Pennsylvania. This file includes five photographs that were taken during the construction.
- (2) February 4, 1918. A technical report by Mr. Arthur T. Safford, Consulting Engineer, Lowell, Massachusetts, regarding the safety and capacity of the unfinished dam to pass the oncoming spring flood.
- (3) May 6, 1952. A petition by the Granite State Electric Co. to the New Hampshire Water Resources Board for reconstruction and repairs of the dam. This petition was granted by order of the New Hampshire Water Resources Board on June 16, 1952. The letter was signed by Mr. L. R. Frost, Water Resources Engineer.
- (4) October, November, 1952. Five large photographs taken during the reconstruction of the dam.
- (5) May 20, 1968. A description of properties in the towns of Canaan and Hanover proposed to be deeded to the State of New Hampshire, including Goose Pond.
- (6) 1969. An act by the general court authorizing the New Hampshire Water Resources Board to acquire the dam and water rights of Goose Pond.

(7) March 15, 1974. Five photographs for the Corps of Engineers' inventory program. No copy of the inventory program was available.

The following files at the New Hampshire Water Resources Board contain important hydrological data and hydraulic computations:

- (1) 1915. The maximum flood discharges from 1895 to 1915, on the Connecticut River drainage area.
- (2) July 8, and 9, 1915. The flood discharge curves.
- ( 3) November 10, 1933. The watershed and storage capacities and a plan of operation of the Mascoma River storage system, including Goose Pond.
- (4) 1952-1953. Several sheets of hydraulic analyses by Mr. F. C. Moore, Civil Engineer.
- (5) 1953-1961. Discharge ratings tabulated by Mr. L. D. Pierce, New England Power Service Co.
- (6) 1962. Profiles at Goose Pond Dam.
- (7) September 18, 1967. Ten-day elevations of the Goose Pond reservoir.
- (8) 1924-1969. Snow depth graphs from November to May 1 of each year.

#### 2. Copies of Past Inspection Reports

Copies of the following reports are included with this report:

- (1) October 17, 1919, by Mr. Robert E. Barrett, General Manager, Connecticut River.
- (2) July 21, 1936, by the New Hampshire Water Resources Board, two pages.
- ( 3) October 31, 1938, by the New Hampshire Water Control Commission, initialed by AAN & RLT, two pages.
- ( 4) December 31, 1960, data sheet by the Granite State Electric Co.

#### 3. Drawings

The New Hampshire Water Resources Board has the following prints showing the layout of the dam, sections, and details. Numbers (2) through (7) were made from June 12, 1917, to June 12, 1918, by the Mascoma River Improvement Company, Engineering Department, Turners Falls' office. Numbers (8) through (13) were made in 1952 by the New England Power Service Company, Boston, Massachusetts.

- (1) July, 1915, C-678, Goose Pond Plan (with some contours).
- ( 2) F-2114 Details of Earth Embankment at Goose Pond Dam.
- (3) F-2178, F-2179, and F-2180 Embankment Sections.
- (4) F-2115, F-2116, F-2117, F-2118, and F-2119 General Layout, Bulkhead, Spillway, and Sluiceway Details.
- (5) B-57, B-58, B-61, and B-62 Plan of Road, Floodgate, Alternate Spillway, Plans, Profiles, and Sections.
- (6) L-25, L-26, L-27 (L-2121, L-2122, L-2254) Details of Rack Bars, Reinforcing of Temporary Gate Opening.
- (7) September, 1928, E-2969; and without a date, L-2110 and E-4685 Profiles at Goose Pond Dam, Clean-out Basins.
- (8) \*H-13823, H-13824, H-13825, H-13831, and H-13836 Spillway Changes.
- (9) H-1037 Topography of Goose Pond Dam and Vicinity.
- (10) \*H-13805 Repairs to be Made to Dike.
- (11) D-4681, LS-3087 Rack Details, Steel Nosing Pieces.
- (12) January 17, 1944 D-3740 Goose Pond Property and Dam, by the Mascoma River Improvement Co.
- (13) January 31, 1978 F-2177 Goose Pond Dam Plan, Profile, and Sections, by the Mascoma River Improvement Co., Engineering Department.

<sup>\*</sup>Reduced copies of drawings are included with this report.

EXCERPT from letter of Robert E. Barrett, General Manager, Connecticut River Conservation Company, Greenfield, Mass., October 17th, 1919. Original letter filed in connection with Grafton Pond file.

#### GOOSE POND -

On September 24th Goose Pond was visited. This dam is built of earth with a concrete core wall. The exposed portion of the core wall was in first-class condition, there being no evidence of settlement or bulging. No cracks were visible. A good growth of grass was on the downstream embankment and there was no evidence of washing. The heavy riprap on the upstream face of the dam was in good condition except a portion fifty feet long westerly from the spillway where the stone had caved in a foot or more due to the fine gravel upon which it was laid being washed out.

The caretaker was placing additional riprap upon this section and was going to fill up to the original surface of the riprap. An open tile drain was being laid at the toe of the downstream embankment on the westerly side. The downstream slope showed no evidence of sloughing and was in first-class condition.

The water stood at gage 8.7; full pond is gage 23.5. This reservoir was filled to overflowing on April 6th and the gate tender recorded a maximum depth of 16 inches over the spillway in the Spring. There was no floating debris in front of the dam. A large number of floating logs and stumps were removed from in front of the dam during the high water in the Spring by the use of the derrick over the spillway.

With the repairs to the riprap and the laying of the open tile drain, both of which should be completed by the middle of October, the dam will be in first-class condition,

\* October 16th. This work is now practically completed.

## NEW HAMPSHIRE WATER RESOURCES BOARD

## INVENTORY OF DAMS AND WATER POWER DEVELOPMENTS

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#### PUBLIC SERVICE COMMISSION OF NEW HAMPSHIRE—DAM RECORD I-5276 TOWN TOWN STATE 36.01 CANAAN NO. 1 NO. RIVER STREAM Coose Pond DRAINAGE POND AREA 15 Sq. Mi. AREA DAM FOUNDATION TYPE Earth Dyke Cement'Core. NATURE OF MATERIALS OF CONSTRUCTION Concrete, Earth PURPOSE POWER—CONSERVATION—DOMESTIC—RECREATION—TRANSPORTATION—PUBLIC UTILITY OF DAM HEIGHTS, TOP OF TOP OF DAM TO DAM TO BED OF STREAM 23.57 SPILLWAY CRESTS 51 SPILLWAYS, LENGTHS LENGTH of DAM 1200 Approx. DEPTHS BELOW TOP OF DAM 45 FLASHBOARDS TYPE, HEIGHT ABOVE CREST OPERATING HEAD TOP OF FLASHBOARDS CREST TO N. T. W. WHEELS, NUMBER KINDS & H. P. GENERATORS, NUMBER KINDS & K. W. H. P. 90 P. C. TIME H. P. 75 P. C. TIME 100 P. C. EFF. 100 P. C. EFF. REFERENCES, CASES, See Plans PLANS, INSPECTIONS

To the Public Service Commission:

(N. E. Power)

Yes. Will be subject to periodic inspection.

Mascoma River Improvement Co.

The foregoing memorandum on the above dam is submitted covering inspection made July 21, 1936, according to notification to owner dated June 25, 1936, and bill for same is enclosed.

D. Waldo White Chief Engineer

August 6, 1936 Copy to Owner

REMARKS

OWNER:

CONDITION:

MENACE:

Good

# NEW HAMPSHIKE WATER CUNTRUL COMMISSION DATA ON DAMS IN NEW HAMPSHIRE

LOCATION	STATE NO36.91
Town: County	Grafton
Stream Goose Pond	•
Basin-Primary Conn R. Secondary	Mascoma R.
Local Name	3° 51 +2,000 V
7200	16.6-E
Drainage area: Controlled Sq. Mi.: Uncontrolled	Sq. Mi.: Total15 Sq. Mi.
Drainage area: Controlled	1918
Height: Stream bed to highest elev 23.5 ft.: Max. Structur	e 18.5 ft
Cost—Dam Reservoir	
DESCRIPTION E Dyke- Cement Core	
Waste Gates	
Type	
Number Size ft. high x	
Elevation Invert: Total Area	
Hoist	_
Number Materials	
Size ft.: Length ft.: Area	sq. ft.
Embankment	
Type	
Height-Max ft.: Min	
Top-Width: Elev	
Slopes-Upstream on	
Length—Right of Spillway Left of Spillway	•••••••••••••••••••••••••••••••••••••••
Spillway	
Materials of Construction Cement	
Length—Totalft.: Net	45. V
Height of permanent section—max13.5 ft.: Min	ft.
Flashboards—Type	: Height ft.
Elevation—Permanent Crest: Top of	Flashboard
Flood Capacity	cfs/sq. mi.
Abutments	
Materials:	
Materials:	
Headworks to Power Devel.—(See "Data on Power Development")	2
OWNER Mascom Niver Introvement Co.	Lebanon N H
Carolfion Good	
REMARKS GRANTE STATE CLECTRIC (NEES)  Une Conservation	•
B-7	

## DATA ON RESERVOIRS & PONDS IN NEW HAMPSHIRE

LOCATION		•	AT DAM NO	36.01 • •
Town Canaan	: c	County Graf	ton	•••••
Stream Goose Pond	***************************************	••••••	••••	
Basin—Primary Conn	R.	Secondary Masc	oma R.	
Local Name		•••••	•••••	
DRAINAGE AREA				
Controlled Sq. M	Ii.: Uncontrolled	Sq. Mi.: Total		Sq. Mi.
ELEVATION vs. WATER ST	URFACE AREA vs. VO	LUME		
Point	Head Feet	Surface Area Acres		olume ere Ft.
(1) Max. Flood Height (2) Top of Flashboard	s	••••••		
<ul> <li>(3) Permanent Crest</li> <li>(4) Normal Drawdown</li> <li>(5) Max. Drawdown</li> <li>(6) Original Pond</li> </ul>	21.5 Usgs825	555	12,300	0
	: Coef. to change to U		*	
RESERVOIR CAPACITY				
	Total Volume	Usea	ble Volume	
Drawdown Volume	ft	. ft.	ft. ac. ft.	
Acre ft. per sq. mi.		• • • • • • • • • • • • • • • • • • •		
Inches per sq. mi. USE OF WATER	Conservation	A		
OWNER Massoms Ri	ion Improvement Co	. Leb	anon N H	
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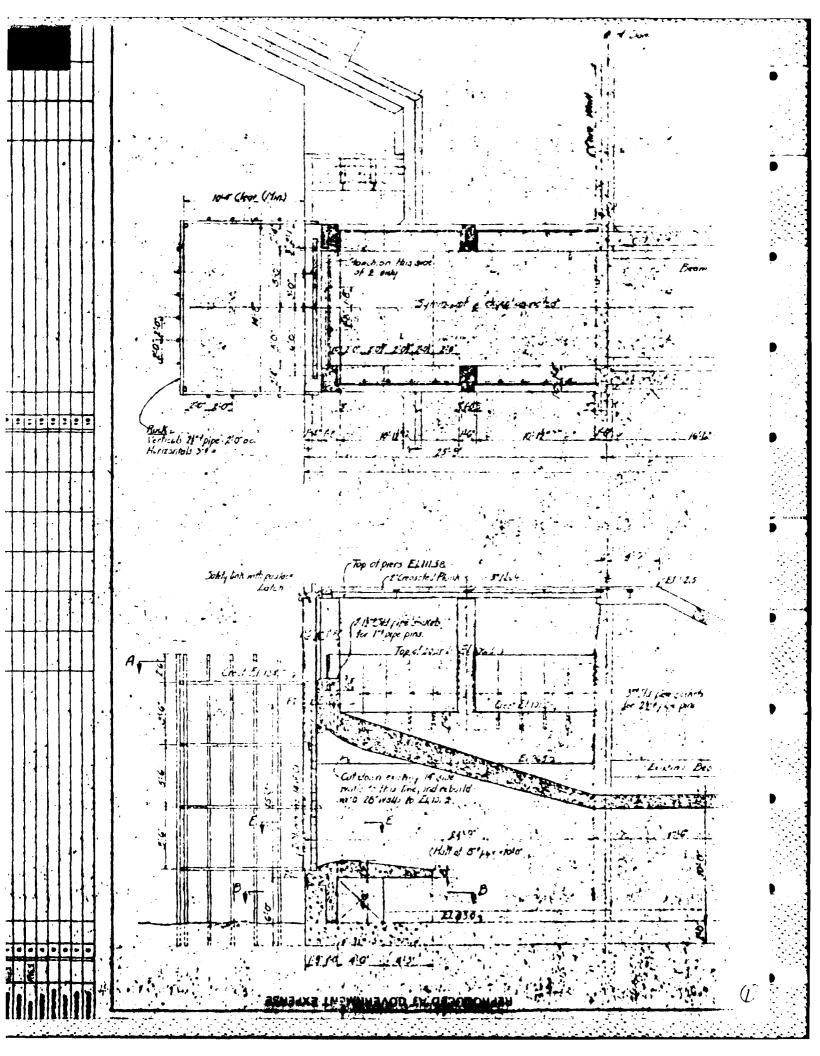
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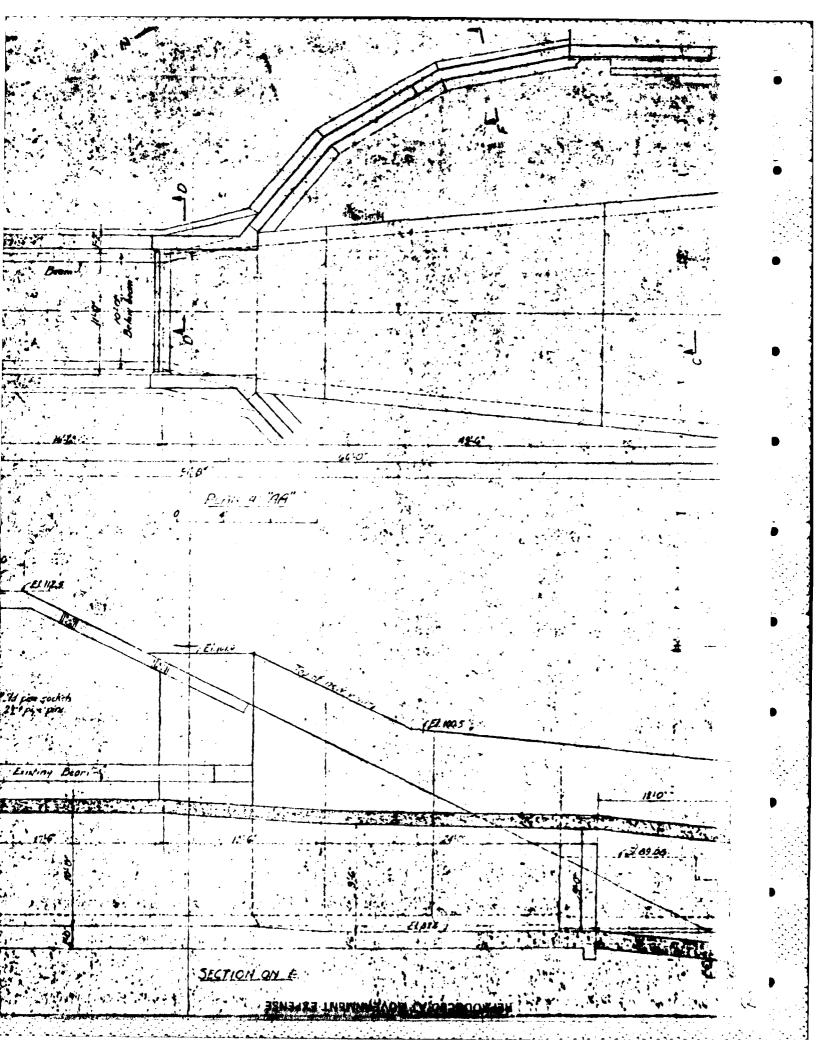
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Canable Lanover [6] Post office Lebanon, N.H.  Canable Lanover [6] Post office Lebanon, N.H.  New Hampshire  No. 15.7 [50] Normal Full [21.5 [6] Centry (acc 1970   110.5 [6] Centry	, PATING COMPANY	Granite State	Flectric Company		
Canable Lanover [6] Post office Lebanon, N.H.  Canable Lanover [6] Post office Lebanon, N.H.  New Hampshire  No. 15.7 [50] Normal Full [21.5 [6] Centry (acc 1970   110.5 [6] Centry					
EMULIC DATA  ANTIONS TOP OF DAMA 27.5 (A) (B) TOP OF BOARDS 21.5 (C) NORMAL FULL 21.5 (O) CREST (SEE STEM SILE)  FIRST FOR AREA 27.5 (A) (B) TOP OF BOARDS 21.5 (C) NORMAL FULL 21.5 (O) CREST (SEE STEM SILE)  FOR OF DAMA 27.5 (A) (B) TOP OF BOARDS 21.5 (C) NORMAL FULL 21.5 (O) CREST (SEE STEM SILE)  FOR IT FOR AREA CO. (F) WINIMUM VARIET O. (G) MINIMUM POSITRE O.  ROTE: ELEVATIONS ARE ON GAGE DATUM: ZERO BOARD ACRE-FEET  FULL FORD AREA 668 ACRES  MAX. ROMAL DRANDOWN 21.5 FT.; VOLUME 11688 ACRE-FEET  MAX. POSSIBLE DRANDOWN 21.5 FT.; VOLUME 11688 ACRE-FEET  (I) COUNTAINT TO 650,600 ERM ON THE FOLLOWING PLANTS: NO. 11  EQUIVALENT TO 3.80 SILLION GALLONS  PRACE RESERVOISS ABOVE ACRES DRAINAGE AREA SO.MI.; USABLE VOLUME ACRES-FE  LOCATION GADES DRAINAGE AREA SO	^	æa % Hanover	(a) POST OFFICE	Lebanon, N.H.	
ACTIONS  FOR POINT AND AREA  15.7  SQUIN. (H) HET DRAILMOSE AREA  ACTIONS  FOR OF DAYS 27.5 (A) (a) TOP OF TOLDES 21.5  (b) NORMAL FULL 21.5  (c) NORMAL FULL 21.5  (d) CREST (SEE THEN ITTEL 11101) 25.1  REGISTEL CHARLOS ARE OF GAGE DATON;  ERROR ELEVATIONS ARE OF GAGE DATON;  REGISTEL CONTROL DATON  MIX. GRADE DARAGOM 21.5  FT.; VOLUME 11688  ACRE-FEET  MIX. FOR STREED DARAGOM 21.5  FT.; VOLUME 11688  ACRE-FEET  MIX. FOR STREED DARAGOM 21.5  FT.; VOLUME 11688  ACRE-FEET  MIX. FOR PLANE ON THE FOLLOWING FLANTS:  NO. 14  EQUIVALENT TO 3.80  SILLION SALLOWS  REGISTEROUS SROVE  LOCATION  GROSS DRAILMOSE AREA  SQUIN.; USABLE VOLUME  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS:  DOCATION  GROSS DRAILMOSE AREA  SQUIN.; USABLE VOLUME  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS:  PLOCATION  GROSS DRAILMOSE AREA  SQUIN.; USABLE VOLUME  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS:  PLOCATION  GROSS DRAILMOSE AREA  SQUIN.; USABLE VOLUME  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS:  PLOCATION  GROSS DRAILMOSE AREA  SQUIN.; USABLE VOLUME  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS:  PLOCATION  GROSS DRAILMOSE AREA  SQUIN.; USABLE VOLUME  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS:  PLOCATION  GROSS DRAILMOSE AREA  SQUIN.; USABLE VOLUME  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS:  STREED ON THE FOLLOWING FLANTS  ACRE-FE  MIX. FOR STREED ON THE FOLLOWING FLANTS  STREED ON THE FOLLOWING FLANTS  B-9  TERMINS & MIX. SUBDRESS STREED ON THE FOLLOWING  ACRE-FE  ATTERIOR OF THE FIRST ON THE FOLLOWING FLANTS  SOUND THE FOLLOWING FLANTS  ACRE-FE  ACRE-FE  ACRE-FE  ACRE-FE  B-9  TERMINS & MIX. SUBDRESS STREED ON THE FOLLOWING  ACRE-FE  ACRE-FE  ACRE-FE  B-9  TERMINS & MIX. SUBDRESS STREED ON THE FOLLOWING FLANTS  ACRE-FE  ACRE-FE  ACRE-FE  ACRE-FE  B-9  TERMINS & MIX. SUBDRESS ACRE-FE  ACRE-FE  ACRE-FE  ACRE-FE  B-9  TERMINS & MIX. STREED ON THE FOLLO	Grafton	I HAIOVOI	(D) STATE	New Hampshire	
15.7   10.41.   10.5	IVER Goose Po	ond Brook - Mascoma Riv	PET (F) MILES ABOVE MOUTH	(DAM) 8.6 (above Masc	oma Dam)
ACRE-FET  LOCATION  CONTROL STANDARD AREA  CONTROL STANDARD CONTROL STANDARD STANDARD STANDARD STANDARD STANDARD AREA  CONTROL STANDARD CONTROL STANDARD	ROSS DRAINAGE AREA	15.7 s	.MI. (H) HET DRAIMAGE AREA	15.7	SQ.MI.
TOP OF DAY 27.5 (A) (B) TOP OF BOARDS 21.5 (C) MORMAL FULL 21.5 (D) CREST (REE ITEM (III) 20.4  MINIMUM NORMAL O (F) MINIMUM USABLE O (G) MINIMUM POSSIBLE O COMMINIMUM NORMAL O (F) MINIMUM NORMAL O					·
TOP OF DAM. 27.5 (A) (B) TOP OF BOARDS 21.5 (C) MORMAL FULL 21.5 (D) CREST (SEE ITEM (III) 360 MINIMUM MORMAL Q (F) MINIMUM WORMAL Q (G) MINIMUM POSSIBLE Q (C) MINIMUM POSSIBLE Q (G) CREST (SEE ITEM (III) 360 MINIMUM MORMAL Q (F) MINIMUM WORMAL Q (G) MINIMUM POSSIBLE Q (G) CREST (SEE ITEM (III) 360 MINIMUM MORMAL Q (G) MINIMUM WORMAL Q (G) MINIMUM POSSIBLE DAWNOOM 21.5 (F): VOLUME 11688 ACRE-FEET (G) COMMAL DAWNOOM 21.5 (F): VOLUME 11688 ACRE-FEET (G) COUNTAINT TO 3.80 BILLION CALLONS  WAX. POSSIBLE DAWNOOM 21.5 (F): VOLUME 11688 ACRE-FEET (G) COUNTAINT TO 3.80 BILLION CALLONS  WAX. POSSIBLE DAWNOOM 21.5 (F): VOLUME 11688 ACRE-FEET (G) COUNTAINT TO 3.80 BILLION CALLONS  WAX. POSSIBLE DAWNOOM 21.5 (F): VOLUME 11688 ACRE-FEET (G): COUNTAINT TO 3.80 BILLION CALLONS  WAX. POSSIBLE DAWNOOM 21.5 (F): VOLUME 11688 ACRE-FEET (G): COUNTAINENT TO 3.80 BILLION CALLONS  WAX. POSSIBLE DAWNOOM 21.5 (F): VOLUME 11688 ACRE-FEET (G): COUNTAINENT TO 3.80 BILLION CALLONS  WATCHIAL EARLY VOLUME ACRE-FEE (G): COUNTAINENT ACRE-FEE (G): COUNTAINENT TO 3.80 BILLION CALLONS  WATCHIAL EARLY VOLUME ACRE-FEE (G): COUNTAINE LENGTH 1.22hO FT. (G) MIX.NT. 11 (A) FILLUMY (h): COUNTAINENT TO 10-0" Crest © F1, 19.5 SEARCHOOT Type 10'-0" Crest © F1, 19.5 SEARCHOOT Type 10'-0" Crest © F1, 19.5 (SOE IV below)  FLASHBOARDS PIN Type 36'-5" ROOTED S'-0" High PIN Type 36'-5" Crest © F1, 16.5 PIN Type 36'-5" ROOTED S'-0" High PIN TYPE 36'-5" ROOTED S'-	<b>!</b>				
TOP OF DAY 27.5 (A) (B) TOP OF BOARDS 21.5 (C) MORMAL FULL 21.5 (D) CREST (REE ITEM (III) 250 (D	MAULIC DATA			•	
ATTOMS   100 of pan   27.5 (A) (s) TOP OF BOADDS   21.5 (c) NORMAL FULL   21.5 (d) CREST (SEE TYEN THE)   20 of pan   27.5 (A) (s) TOP OF BOADDS   21.5 (c) MINIMUM POSSIBLE   0   0   0   0   0   0   0   0   0					יסנ 🖘 יסנ
Rote: ELEVATIONS ARE ON   Cage	ATIONS	(.)	, a.	<b>.</b>	
Rote: ELEVATIONS ARE ONGageDATUM;	TOP OF DAN 27.5	(A) (B) TOP OF BOARDS 21.	(c) NORMAL FULL	1.5 (D) CREST (SEE ITE	M
ACRE-FERTY OND AREA 668 ACRES MAX. HORNEL DRAFFORM 21.5 FT.; VOLUME 11688 ACRE-FEET; .509 acr13.96 INS. ON 15.7 SO.MI MAX. HORNEL DRAFFORM 21.5 FT.; VOLUME 11688 ACRE-FEET MAX. POSSIBLE DRAFFORM 21.5 FT.; VOLUME 11688 ACRE-FEET MAX. POSSIBLE DRAFFORM 21.5 FT.; VOLUME 11688 ACRE-FEET  (i) COULVALENT TO 650,600 FT. OLD OLD FT.; VOLUME 11688 ACRE-FEET  (ii) COULVALENT TO 3.80 BILLION CALLONS  NO. 4 ACRE-FE  LOCATION NOTH GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  COCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  MATERIALEARTH & CONCRETS) TYPEROILED FILL (c) OVERALL LENGTH 1,210 FT. (e) MAX. NT. 111 (A) F  PIN TYPE 101-0" Crest © F1. 19.5  Stanchion Type 101-0" Crest © F1. 19.5  Stanchion Type 101-0" Crest © F1. 3,5 (See IV below)  FLASHBOARDS FIN TYPE - 361-51" SOCRES 51-0" High  PIN Type - 101-0" Boards 21-0" High  Stanchion Type - 101-0" Wide x 151 (approx.) High (See IV below)  CARTS 2 - 11 x 11 Gates Sill © F1 2.0 (83,0)  TERMANS & MISC. Submerged stop logs 101 x 151 approx. Sill © CH 3.5  B-9	AINIMUM NORMAL <u>O</u>	(F) MINIMUM USABLE	(G) MINIMUM POSSIBLE	E	
		Caro	85 0 ab	017.0	
######################################	Hoto: ELEVATIONS	ARE ON GAGE DATUM;	ZERO = U5.0 au	o tum	
TOTAL POND AREA 668 ACRES MAX. MORNAL DARBOONN 21.5 FT.; VOLUME 11688 ACRE-FEET; 509 BCF 13.96 INS. ON 15.7 SQ.MI MAX. MORNAL DARBOONN 21.5 FT.; VOLUME 11688 ACRE-FEET MAX. POSSIBLE ORANDONN 21.5 FT.; VOLUME 11688 ACRE-FEET  (1) EQUIVALENT TO 650,600 KEM ON THE FOLLOWING PLANTS: NO. II  EQUIVALENT TO 3.80 BILLION GALLONS  PRACE RESERVOIRS ABOVE LOCATION NOTE GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FEE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE NOTE OF THE PLANTAGE AREA SO.MI.; USABLE VOLUME ACR		٠ ,	TOCAT D	acum	•
TOUL FORD AREA 668 ACRES  MAX. MARIA DARFORM 21.5 FT.; VOLUME 11688 ACRE-FEET; 509 BCF 13.96 INS. ON 15.7 SQ.MI  MAX. HORRIE DARFORM 21.5 FT.; VOLUME 11688 ACRE-FEET  MAX. POSSIBLE DRAWGORN 21.5 FT.; VOLUME 11688 ACRE-FEET  (I) EQUIVALENT TO 650,600 KPM ON THE FOLLOWING PLANTS: NO. II  EQUIVALENT TO 3.80 BILLION GALLONS  MAGE RESERVOIRS ABOVE  LOCATION NOTE GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FEE  LOCATION GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE  LOCATION GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE  MATERIALEARTH & CONCRETE: TYPE ROlled Fill (c) OVERALL LENGTH 1,2LO FT. (d) MAX. MT. LII (A)  SPILLWAY (161-57 © E1. 21.5 effective length) Pin Type 361-57 Crest © E1. 16.55  Pin Type 101-07 Crest © E1. 3.5 (See IV below)  FLASHBOARDS PAIN TYPE - 361-51 BOARDS 21-07 High  Pin Type - 361-57 BOARDS 21-07 High  Pin Type - 101-07 BOARDS 21-07 High  Stanchion Type 101-07 BOARDS 21-07 High  Stanchion Type - 101-07 Wide x 151 (approx.) High (See IV below)  GATTS 2 - 11 X 11 Gates Sill © E1 2.0 (83.0)  TERMAYS 4 MISC. Submerged stop logs 101 X 151 approx. Sill © CH 3.5  B-9					
MAX. NORMAL DRANDOWN 21.5 FT.: VOLUME 11688 ACRE-FEET  MAX. POSSIBLE DRANDOWN 21.5 FT.: VOLUME 11688 ACRE-FEET  MAX. POSSIBLE DRANDOWN 21.5 FT.: VOLUME 11688 ACRE-FEET  (i) COULVALENT TO 650,600 KMH ON THE FOLLOWING PLANTS: NO. 1  FOUNTALENT TO 650	: AGE	668			
	FULL POND AREA	27 5	11688 ACRESERY . 50	9 acr13.96 INS. ON 1	5.7 sq.mi.(1
NO. 14  RACE RESERVOIRS ABOVE LOCATION NOTE GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION NOTE GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE		21.5	1688 ACREAGEST		
(1) EQUIVALENT TO 650,600 KEN ON THE FOLLOWING PLANTS: No. 4  EQUIVALENT TO 3.80 BILLION CALLONS  RAGE RESERVOIRS ABOVE LOCATION NOTE GROSS DHAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS OBTAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS OBTAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  MATERIALEARTH & CONCRETE, TYPEROILED FILL (c) OVERALL LENGTH 1,240 FT. (d) MAX. HT. 11 (A) F 5*ILLEAY (161-5* © El. 21.5 effective length) Pin Type 361-5* Crest © El. 16.5  Pin Type 101-0* Crest © El. 19.5  Stanchion Type 101-0* Crest © El. 3.5 (See IV below)  FLASHBOAROS FIN Type - 36*-5* Roards 5*-0* High Pin Type - 101-0** Boards 2*-0** High Stanchion Type - 101-0** Boards 2*-0** High Stanchion Type - 101-0** Boards 2*-0** High Stanchion Type - 101-0** Wide x 15* (approx.) High (See IV below)  FARMYS & MISC. Submerged stop logs 10* x 15* approx. Sill © CH 3.5  B-9			1688 ACRE FEET		
RACE RESERVOIRS ABOVE LOCATION NOME GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS ORAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS ORAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS ORAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION FIND 101-5" GEL 21.5 effective length) Pin Type 361-5" Crest GEL 16.5  Pin Type 101-0" Crest GEL 19.5 Stanchion Type 101-0" Crest GEL 19.5 Stanchion Type 101-0" Crest GEL 19.5 Stanchion Type - 101-0" Boards 51-0" High Pin Type - 101-0" Boards 21-0" High Stanchion Type - 101-0" Wide x 15' (approx.) High (See IV below)  FLASHBOARDS 2 - L' x L' Gates Sill GEL - 2.0 (83.0)  TERMYS A MISC. Submerged stop logs 10' x 15' approx. Sill GCH 3.5  B-9	MAX. POSSIBLE DRAWD	70LUNE			
RAGE RESERVOIRS ABOVE LOCATION NOTICE GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  MATERIALEARTH & CONCRETE) TYPEROILED FILL (c) OVERALL LENGTH 1,210 FT. (d) MAX. HT. 11 (A) F SPILLWAY (161-57 GEL. 21.5 effective length) Pin Type 361-5" Crest & El. 16.5  Pin Type 101-0" Crest & El. 19.5  Stanchion Type 101-0" Crest & El. 3.5 (See IV below)  FLASHBOARDS PIN TYPE - 36'-5" BOARDS 5'-0" High Pin Type - 101-0" BOARDS 2'-0" High Stanchion Type - 101-0" Wide x 15' (approx.) High (See IV below)  CATES 2 - 1 x 1 Gates Sill & El 2.0 (83.0)  TERMAYS 4 MISC. Submerged stop logs 10' x 15' approx. Sill & CH 3.5  B-9	(1) COLLIVE ENT TO	650.600 KWH ON THE FOLLOW	ING PLANTS:	No. 4	·
RACE RESERVOIRS ABOVE  LOCATION NONE  GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  MATERIALEARTH & CONCretes) TYPEROILED FILL (c) OVERALL LENGTH 1,210 FT. (b) MAX. HT. L1 (A) FT SPILLWAY (161-5" © E1. 21.5 effective length) Pin Type 36'-5" Crest © E1. 16.5  Pin Type 10'-0" Crest © E1. 3,5 (See IV below)  FLASHBOARDS PIN Type - 10'-0" Boards 5'-0" High PIN Type - 10'-0" Boards 5'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - 1' X 1' Gates Sill © E1 2.0 (83.0)  TERMAYS 4 MISC. Submerged stop logs 10' x 15' approx. Sill © CH 3.5  B-9	(1) EGOLANTENI 10				
CACE RESERVOIRS ABOVE  LOCATION NONE  GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION DRAIN GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION DRAIN GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE  ACRE	FOUTVALENT TO	3.80 BILLION GALLONS		•	
LOCATION NOTE GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE NUMBER (1661-5" @ E1. 21.5 effective length) Pin Type 36'-5" Crest @ E1. 16.5 Pin Type 10'-0" Crest @ E1. 19.5  Stanchion Type 10'-0" Crest @ E1. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Roards 5'-0" High Pin Type - 10'-0" Boards 2'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - 11' x 11' Gates Sill @ E1 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill @ CH 3.5  B-9					
LOCATION NOTE GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE NUMBER (1661-5" @ E1. 21.5 effective length) Pin Type 36'-5" Crest @ E1. 16.5 Pin Type 10'-0" Crest @ E1. 19.5  Stanchion Type 10'-0" Crest @ E1. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Roards 5'-0" High Pin Type - 10'-0" Boards 2'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - 11' x 11' Gates Sill @ E1 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill @ CH 3.5  B-9					
LOCATION NOTE GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SO.MI.; USABLE VOLUME ACRE-FE NUMBER (1661-5" @ E1. 21.5 effective length) Pin Type 36'-5" Crest @ E1. 16.5 Pin Type 10'-0" Crest @ E1. 19.5  Stanchion Type 10'-0" Crest @ E1. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Roards 5'-0" High Pin Type - 10'-0" Boards 2'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - 11' x 11' Gates Sill @ E1 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill @ CH 3.5  B-9	POTUE DESEGNUTOS TO	OVE		•	
GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE MATERIALEARTH & CONCRETE: 12.5 effective length) Pin Type 36'-5" Crest & El. 16.5 Pin Type 10'-0" Crest & El. 19.5 Stanchion Type 10'-0" Crest & El. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Boards 5'-0" High Pin Type - 10'-0" Boards 2'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - h' x h' Gates Sill & El 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill & GH 3.5  B-9	LOCATION	ONE GROSS DRAINAGE ARI	EA SQ.MI.; USA	BLE VOLUME	ACRE-FEET
GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE LOCATION GROSS DRAINAGE AREA SQ.MI.; USABLE VOLUME ACRE-FE MATERIAL Earth & Concretes) Type Rolled Fill (c) OVERALL LENGTH 1,210 FT. (d) MAX.HT. Lil (A) FT. SPILLWAY (1601-5" © El. 21.5 effective length) Pin Type 36'-5" Crest © El. 16.5 Pin Type 10'-0" Crest © El. 19.5 Stanchion Type 10'-0" Crest © El. 3,5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Boards 5'-0" High Pin Type - 10'-0" Boards 2'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - 1' x 1' Gates Sill © El 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill © CH 3.5  B-9	LOCATION	GROSS DRAINAGE AR	SQ.MI.; USA	BLE VOLUME	ACRE-FEET
ACRE-FE  MATERIALEARTH & CONCRETE B) TYPE Rolled Fill (c) OVERALL LENGTH 1,240 FT. (D) MAX.HT. Lil (A) F  SPILLWAY (16'-5" © El. 21.5 effective length) Pin Type 36'-5" Crest © El. 16.5  Pin Type 10'-0" Crest © El. 19.5  Stanchion Type 10'-0" Crest © El. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Boards 5'-0" High  Pin Type - 10'-0" Boards 2'-0" High  Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  CATES 2 - 1' x 1' Gates Sill © El 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill © CH 3.5  B-9	LOCATION	GROSS DRAINAGE AR	EASQ.M1.; USA	ABLE VOLUME	ACRE-FEET
MATERIALEARTH & Concrete:  MATERIALEARTH & Concrete:  MITERIALEARTH & MITERIALEARTH	LOCATION	GROSS DRAINAGE AR	EASQ.M1.; USA	BLE VOLUME	ACRE-FEET
MATERIALEARTH & Concretes) Type Rolled Fill (c) OVERALL LENGTH 1.2LO FT. (d) MAX. HT. Lil (A) FSPILLWAY (Li6'-5" © El. 21.5 effective length) Pin Type 36'-5" Crest © El. 16.5  Pin Type 10'-0" Crest © El. 19.5  Stanchion Type 10'-0" Crest © Fl. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Boards 5'-0" High  Pin Type - 10'-0" Boards 2'-0" High  Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - L' x L' Gates Sill © El 2.0 (83.0)  TERMAYS A MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9					
MATERIALEARTH & Concrete: Type Rolled Fill (c) OVERALL LENGTH 1.2LIO FT. (b) MAX. HT. LII (A) FT. SPILLWAY (LIG-5" © E1. 21.5 effective length) Pin Type 36'-5" Crest © E1. 16.5  Pin Type 10'-0" Crest © E1. 19.5  Stanchion Type 10'-0" Crest © F1. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Boards 5'-0" High  Pin Type - 10'-0" Boards 2'-0" High  Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - L' x L' Gates Sill © E1 2.0 (83.0)  TERMAYS A MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9					
MATERIALEARTH & Concrete: Type Rolled Fill (c) OVERALL LENGTH 1.2LIO FT. (b) MAX. HT. LII (A) FT. SPILLWAY (LIG-5" © E1. 21.5 effective length) Pin Type 36'-5" Crest © E1. 16.5  Pin Type 10'-0" Crest © E1. 19.5  Stanchion Type 10'-0" Crest © F1. 3.5 (See IV below)  FLASHBOARDS Pin Type - 36'-5" Boards 5'-0" High  Pin Type - 10'-0" Boards 2'-0" High  Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  GATES 2 - L' x L' Gates Sill © E1 2.0 (83.0)  TERMAYS A MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9	4	•			
Pin Type 10'-0" Crest © El. 19.5  Stanchion Type 10'-0" Crest © El. 3.5 (See IV below)  FLASHBOARDS  Pin Type - 36'-5" Boards 5'-0" High  Pin Type - 10'-0" Boards 2'-0" High  Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  CATES 2 - h' x h' Gates Sill © El 2.0 (83.0)  TERMAYS A MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9  TERMAYS A MISC. Submerged Stop logs 10' x 15' approx. Sill © GH 3.5	www.Earth &	Concrete ) TYPE Rolled Fi	11(c) OVERALL LENGTH	<u> 1,240 гт. (d) мх. нт 4.</u>	1 (A) FT.
Pin Type 10'-O" Crest © El. 19.5  Stanchion Type 10'-O" Crest © El. 3.5 (See IV below)  FLASHBOARDS  Pin Type - 36'-5" Boards 5'-O" High  Pin Type - 10'-O" Boards 2'-O" High  Stanchion Type - 10'-O" Wide x 15' (approx.) High (See IV below)  CATES 2 - h' x h' Gates Sill © El 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9	SPILLWAY (461	-5" @ El. 21.5 effect:	ive length) Pin Ty	pe 36'-5" Crest 6	E1. 16.5
Stanchion Type 10'-0" Crest © El. 3.5 (See IV below)  FLASHBOARDS  Pin Type - 36'-5" Boards 5'-0" High  Pin Type - 10'-0" Boards 2'-0" High  Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  CATES 2 - h' x h' Gates Sill © El 2.0 (83.0)  TERMAYS * MISC. Submerged stop logs 10' x 15' approx. Sill © CH 3.5  B-9  TES  1 = APPROXIMATE ONLY  1) = NOT AVAILABLE		Pin Type 101-0" Cres	t @ El. 19.5		
Pin Type - 36'-5" Boards 5'-0" High Pin Type - 10'-0" Boards 2'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  CATES 2 - h' x h' Gates Sill @ El 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill @ CH 3.5  B-9  TES  1 = APPROXIMATE ONLY 1) = NOT AVAILABLE		Stanchion Type 10'-0"	Crest @ El. 3.5	(See IV below)	
Pin Type - 10'-0" Boards 2'-0" High Stanchion Type - 10'-0" Wide x 15' (approx.) High (See IV below)  CATES 2 - h' x h' Gates Sill © El 2.0 (83.0)  TERMAYS & MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9  TES    = APPROXIMATE ONLY   NOT AVAILABLE	FLASHBOARDS	Pin Type $= 36!-5"$ Box	erds 5'-0" High		
TERMYS 4 MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9  TES    = APPROXIMATE ONLY   NOT AVAILABLE		Pin Type - 10'-0" Box	ards 2'-0" High		
TERMAYS A MISC. Submerged stop logs 10' x 15' approx. Sill © GH 3.5  B-9  TES  1 = APPROXIMATE ONLY  1) = NOT AVAILABLE		Stanchion Type - 10'-	O" Wide x 15' (appr	ox.) High (See IV	below)
B=9  TES ) = APPROXIMATE ONLY L) = NOT AVAILABLE	GATES 2 -	h'xh' Gates Sill @	El 2.0 (83.0)		
B=9  TES ) = APPROXIMATE ONLY L) = NOT AVAILABLE	<del></del>				
B=9  TES ) = APPROXIMATE ONLY L) = NOT AVAILABLE					
TES   ) = APPROXIMATE ONLY  A) = NOT AVAILABLE	<del></del>				
TES ) = APPROXIMATE ONLY A) = NOT AVAILABLE				411 A M 2 C	
TES  TES  TES  TOTAL  TES  TES  TES  TES  TES  TES  TES  TE	Termays & Kisc.	Submerged stop logs l	יע x 15' approx. S	SIII # OH J.>	
TES  TES  TES  TES  TES  TES  TES  TES			<b>5</b> 0		
TAPPROXIMATE ONLY THE NOT AVAILABLE			B-9		
TAPPROXIMATE ONLY THE NOT AVAILABLE			•		
TAPPROXIMATE ONLY THE NOT AVAILABLE	TES .				
A) = NOT AVAILABLE		4LY			
				•	
19/21/60					•
TA AS OF 12/21/00 NTD. ECON. NO. 300A 012431	TA AS OF 12/31/	/60		HYD. ECON. NO. 366A	012451

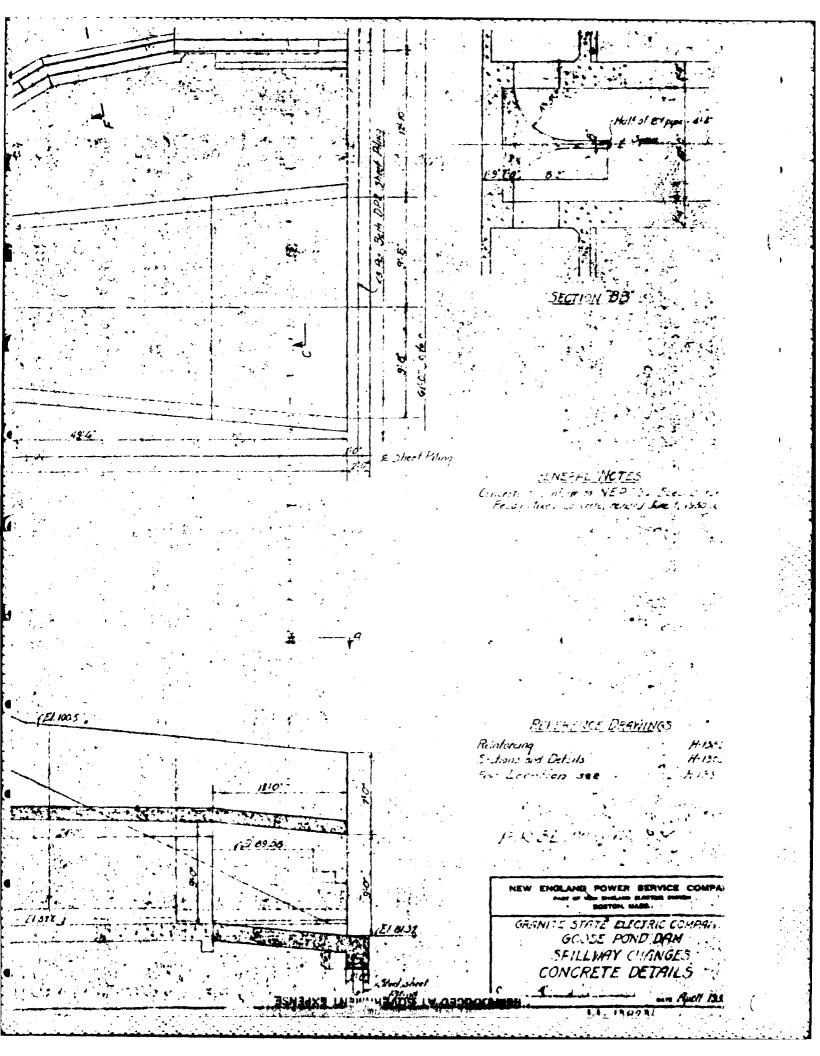
STORAGE RESERVOIR DATA

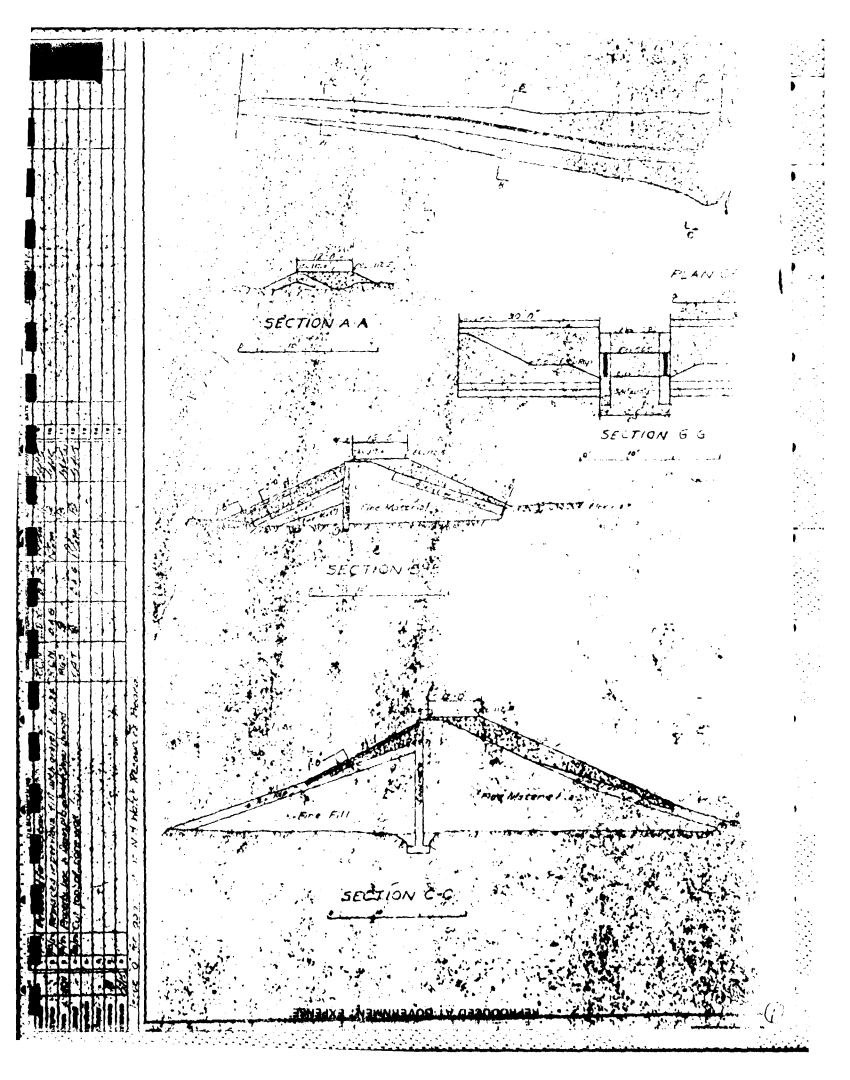
SHEET NO. 2U/

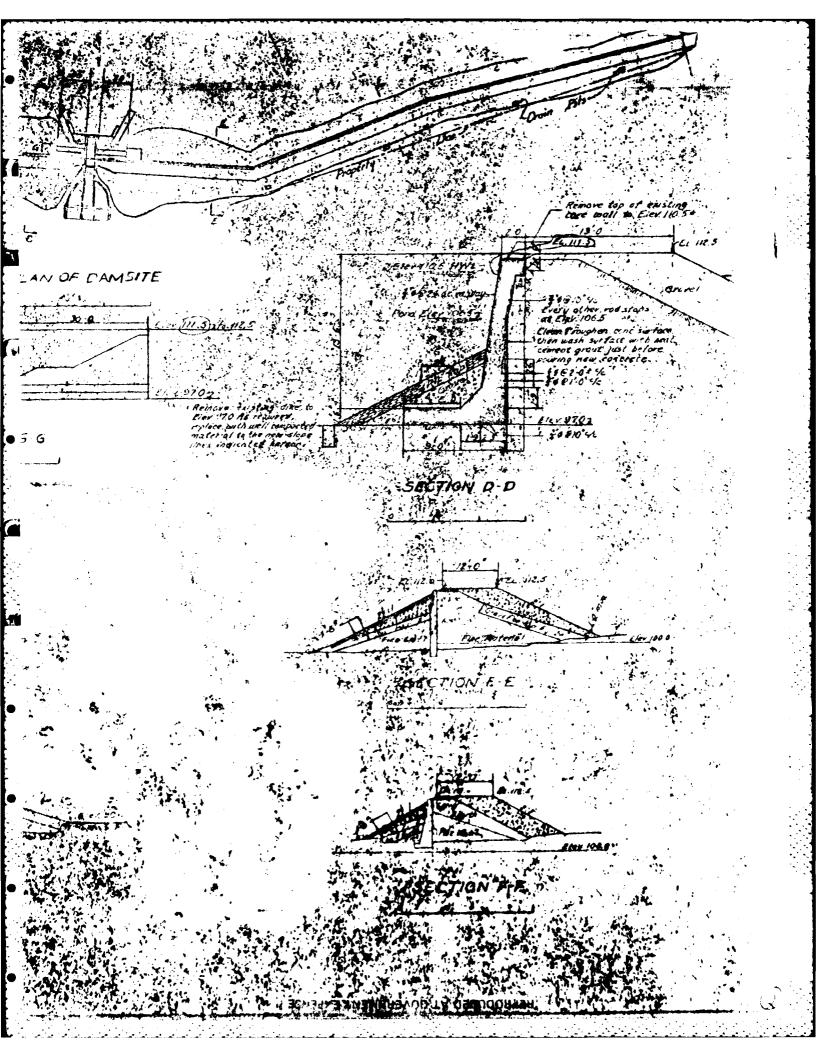
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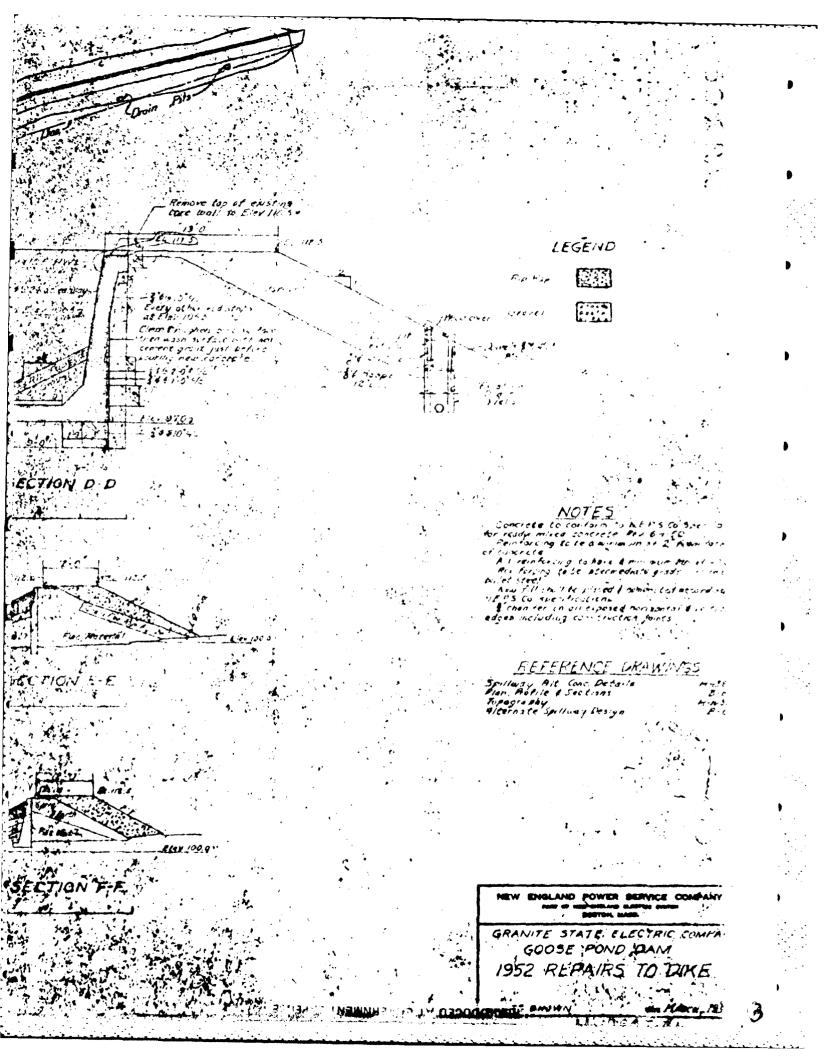


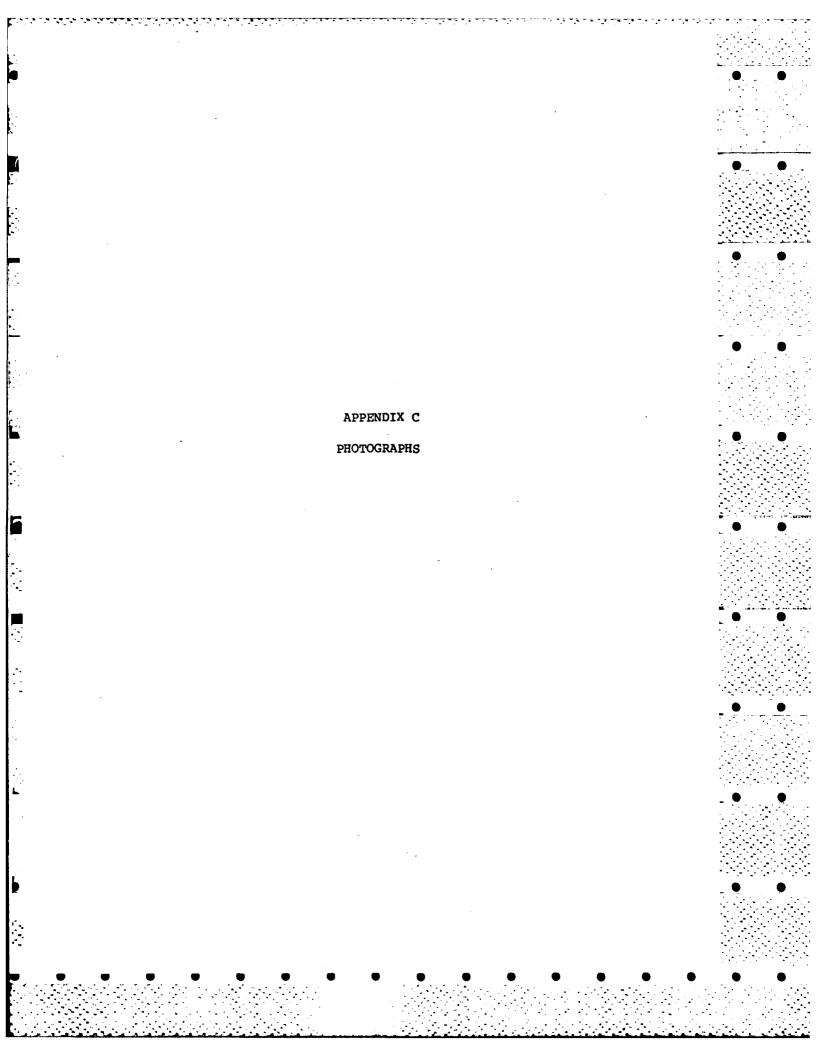










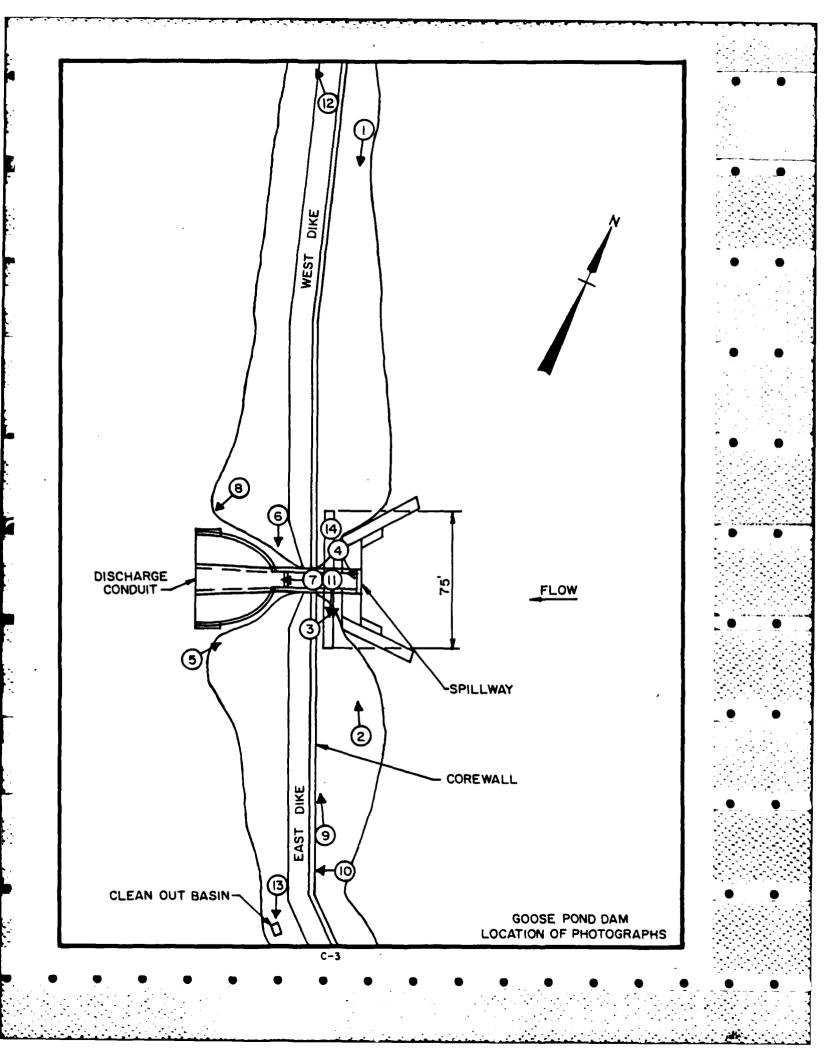


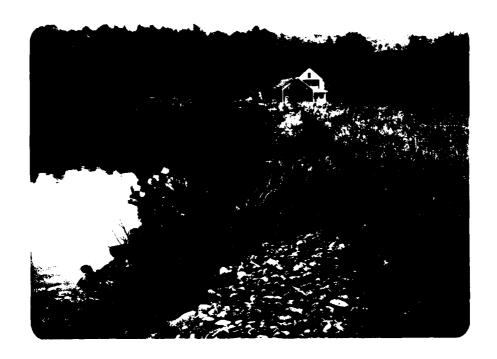
## APPENDIX C

## REPRESENTATIVE PHOTOGRAPHS OF PROJECT

LOCA'	TION PLAN		Page
Plan	1 - Location of Photographs Taken on June	e 8, 1978	C-3
PHOT	OGRAPHS		
No.		Negative No.	Page
1.	Goose Pond Dam, looking east. Showing vegetation on the upstream side of the core wall.	8-10A	C-4
2.	Intake structure with rectangular spillway.	8-6A	C-4
3.	Spillway crest with flashboards in place, looking northwest.	8-8A	C-5
4.	Stop log stanchions on the north side of the intake structure	8-22A	C-5
5.	Buttressed wingwall of discharge channel, looking northwest.	8-18A	C-6
6.	Discharge channel with cross beams, looking east.	8-16A	C-6
7.	Discharge channel showing top of sluice conduit, looking downstream.	8-15A	C-7
8.	Both wingwalls of discharge channel and Goose Pond Brook, looking downstream	. 8-13A	C-7
9.	Erosion of concrete core wall of the east dike.	8-3A	C-8
10.	Cracking and spalling of concrete core wall, east dike.	8-4A	C-8

No.		Negative No.	Page
11.	East dike, showing riprap and concrete core wall near the intake structure.	8-23A	C-9
12.	West dike, showing trees on the downstream slope (left), and bushes on the upstream slope near the west end of the dike.	8-11A	C-9
13.	Clean-out basin near the downstream toe of the east dike.	8-25A	C-10
14.	Gate hoist at the northeast corner of the intake structure, with the crank locked.	8-21A	C-10

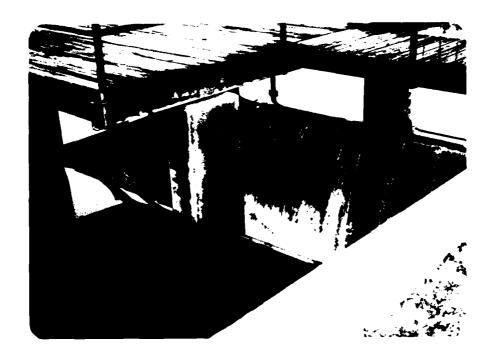




1. Goose Pond Dam, Looking East. Showing Vegetation on the Upstream Side of Core Wall.



2. Intake Structure with Rectangular Spillway.



3. Spillway Crest with Flashboards in Place, Looking Northwest.



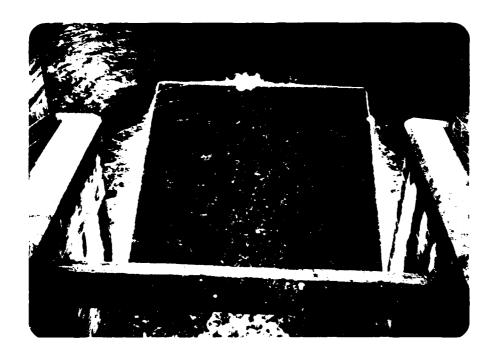
4. Stop Log Stanchions on the North Side of the Intake Structure.



5. Buttressed Wingwall of Discharge Channel, Looking Northwest.



6. Discharge Channel with Cross Beams, Locking Fast.



7. Discharge Channel Showing Top of Cluice Conduit, Looking Downstream.



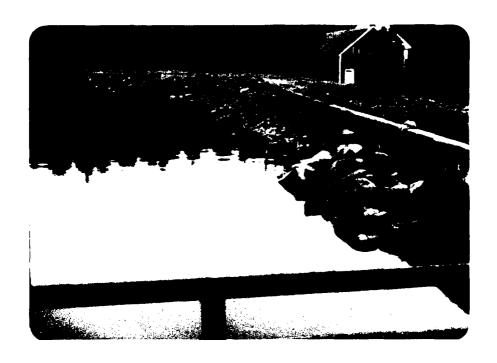
c. th Wingwallo of Dischunge Channel and Boose Fond Frook, Lookeed Downstream.



9. Erosion of Concrete Core Wall of the East Dike.



10. Cracking and Spalling of Concrete Core Wall, East Dike.



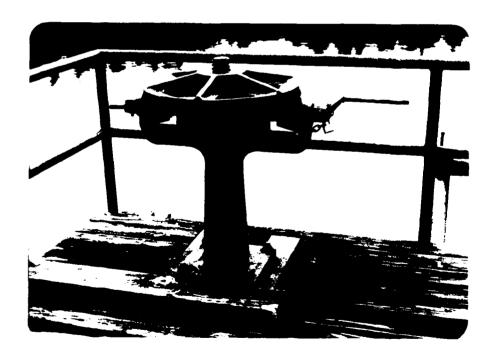
11. East Dike, Showing Rip-Rap and Concrete Core Wall Near the Intake Structure.



12. West Dike, Showing Trees on the Downstream Slope (Left), and Bushes on the Upstream Slope Near the West End of Dike.



13. Clean-out Basin Near the Downstream Toe of the East Dike.



14. Gate Holst at the Northeast Corner of Intake Structure, with the Grank Lockel.

APPENDIX D
HYDROLOGIC & HYDRAULIC COMPUTATIONS

PROJECT EN- 606 (4)

BUBBERT NETIONAL DAM INSP. PROGENIA GOLSE POND DIM

FILE NUMBER Eli- ( ) BHEET NUMBER 1 7 DATE 5-25-12 COMPUTED BY 16. 111

2.210092 216 6/6/10 - Hard Same = 15.7 Experiences The Interest and of forme portal is the astrocked by mountainons to be graphy. He weed from quick Cares Aunni Shed by harbe of Engineers, it its lowered that

Probable marcimum inflow flood PERIC = 1830x 1577 = 28730 275

As a day to the size classification, broke Find Enne is Luge.

necessary for hazard classife intern, ich into into the Category of high hazard dame.

c. Spillway rest Flord (unflow) = 28,730 cls

PROJECT <u>EN-006</u> (4)

BUDDECT GODGE BUD

TEST FLOOD FRUN HYDRUSTAPH

Length of Tale = 35,700'

Difference in Elevation = 1,385' To = Time of Concentration

 $T_{c} = \frac{(35700)^{1.15}}{77\omega \times (1,385)}^{0.35}$ 

= 172015.3 7700 × 15.6

= 1.43 SAY 1.5 hr.

spilling rest inflow flood Peak = 28,730 Cts.

AMMENUIN-W PROJECT EN-006 (4)

FILE NUMBER E/1-000

100 (502/E RUSO

COMPUTED BY PINA

TEST FLOOD THE DIN HYDROGENEH (BASED LINELS DIMENSIONLESS UNIT HYDROGENPH)

Tc = 1.5 hr.

Qp = 28,730 CFS

T(hrs.)	T/1c	9/00	Q(c=s)
.375	0.25	0.05	1,436.5
.75	0.50	0.13	5,171.4
1.125	0.75	0.73	20,972.9
1.50	1.00	1.00	26,730.0
1.975	1.25	0.30	22,984.0
2.25	1.50	0,40	11,492.0
2.625	1.75	0.25	7,182.5
3.00	2.00	0.17	4,334.1

REFER TO PAGE 15 FOR THE PLOT

PROJECT - 11- C' - 1.1

SUBJECT RATTIFIC COL TWO GATE OF EN 1988.

REFERTO TABLE ON PAGE 7

BOTH Chare and good

ELEVATION

F,

83.0

85.00

64.0

27.0 .

168.0

24.0

243.0

71.0

32010

93.0

384,0

950 ...

440.0

17:0

498.0

99.0

552.0

101.0

600.0 608.0

-101.5 1030 5

340.0

104.0

134.0 540.0

155.0

696.0

106.0 107.0

12201C

108.0

744.0

109.0

768.0

110.0

792.0

612.0

111.0

112.0

840.0

FAY, SPOFFORD & THORNDIKE, INC. ENGINEERS PROJECT = M-176

HEET NUMBER

BUBJECT 24 TIMB FOR SIME SPILLYING -

COMPUTED BY

SLEVATION!

12

0.0

0.0

63.0

101.0

11200

13200

210.0

104.0

403.0

105.0

638, D

106.0.

899.0

107.0

1193.0

108.0

1520.0

109.0

1886,0

110.0

226810

111. 0

2688.0

112,0

3108.0

REFERTO THBLE ON PAGE 8

FAY, SPOFFORD & THORNDIKE, INC. ENGINEERS

PROJECT EN-CIA

FILE NUMBER <u>EN-006</u>

SHEET NUMBER <u>1</u>

DATE <u>E-21-1978</u>

BUBJECT RATING FOR FIND SPILLURY

COMPUTED BY 12/11

10 FT 40113

CHECKED BY

ELEVATION		Q
101.0		0 0 4.0
152 . 0		11.0
104.0		18.0
105.0		25.0
158.3		32.0
167.0		390
108.0	•	46.0
169.0		54.0
110.0	•	61.0
111.0	• • • • • • • •	67.0
112.0		75.0

REFER TO TABLE ON PAGE 8.

#### RATING TARLE FROM RECORDS

#### GRANITE STATE ELECTRIC CO. GOOSE POND IMPROVED FLOOD WASTEWAY

Discharge in C.F.S. of both gates for each foot of combined vertical opening E.G. Pond at 98.3; one gate 3' open, one gate 2' open or total-5'; Discharge = 5x66=330 C.E.S.

	•0	•1	•2	•3	•1	•5	•6	•7	.8	•9
83	0	0	0	1	1	1	ı	1	2	2
84 85 86	2	2	4	4 _	lı	5	1 6	1 6	6	7
85	8	8	9	9	10	11	11	12	12	12
86	13	13	15	16	16	17	18	18	19	20
87	21	21	22	23	23 28	23	24	30 24	25	26 31
88	26	27	27	28	28	29	29	.30	30	31
89٠	31	32 36	32 36	33 37	33 37	33 38	34 38 +	34 38	35	35
90 91	36	36	36	37	37	38	38 '	38	39	35 39 43
91	140	40	40	41	41 45 49	41	142	142	43	43
92	44	1,1, 1,8	45	45	45	46	46	47	47	47
93	48	48	49	49	49	50	50	50	51	51
94	52 55	5 <u>2</u> 55_	52 56	53 56	<u>53</u> 57	53 57	54 57	50 54 58	54	55
92 93 94 95 96	55	55	56	56	57	57	57	58	58	47 51 55 58 62 65 69
<b>-96</b>	59	59	59	60	60	60	61	61	61	62
97	62	62 65 69	63	63	63 67	63	64	64	64	65
98	65	65	66	66	67	67	68	68	68	69
_99_	69	69	69	70	70	70	70 7կ	71	71	71_
100	72 75	72 75.	72	73 75	73	73	74	74	74	7 <u>1</u> 7 <u>4</u> 77
101	75	<u>75</u> .	75	75	76	76	76	76	77	77
102	77	78 80	78	78	78	78	79	79	79	80
103	80	80	80	81	81	81	81	82	82	82
104 105	83 85	83 85	8 <u>3</u> 85	83 86	· 83 86	84	84 86	84	814	80 82 85 87
105	85	85	85	86	86	86	86	86	87	87
106	87	88	88	88	88	88	89	89	89	90
107	90	90	90	91	91	91	91	92	92	92 95
108	93	93	94	94	94	94	94	95	95	95
109	96	96	96	96	97	97	97	98	98	98
110	99	99	99	99	100	100	100	101	101	101
111	102	102	102	103	103	104	104	104	104	105
112	105									

#### GRANITE STATE ELECTRIC CO. Goose Pond Dam Discharge Rating, C.F.S. per horizontal foot

Side Spillways, over Clear Concrete Crest at 101.5, 36.4: long. This assumes boards removed to crest; lst. from side spillways, then from end.

Elev.	•0	•1	•2	•3	•4	•5	•6	•7	•8	•9
101						•0	.1	•14	•7	1.1
2	1.5	1.8	2.1	2.4	2.7	3.1	3.4	3.8	4.2	4.6
3	5.0	5.4	5.8	6.2	6.7	7.2	7.6	8.1	8.6	9.1
2 3 4	9.6	10.1	10.6	11.1	11.7	12.3	12.8	13.4	14.0	14.6
105	15.2	15.8	16.4	17.0	17.6	18.3	18.9	19.5	20.1	20.7
6	21.4	22.0	22.7	23.4	24.1	24.8	25.5	26.2	26.9	27.6
	28.4	29.1	29.8	30.6	31.4	32.2	33.0	33.8	34.6	35.4
7 8 9	36.2	37.0	37.8	38.7	39.6	40.5	41.3	42.2	43.1	44.0
9	9. بلباً	45.8	46.7	47.6	48.5	49.4	50.3	51.2	52.1	53.0
цó	54.0	55.0	56.0	57.0	58.0	59.0	60.0	61.0	62.0	63.0
11	64.0	65.0	66.0	67.0	68.0	69.0	70.0	71.0	72.0	73.0
12	74.0	•,,••		• , • •		-, -,	,		,	124-

End Spillway, over Concrete crest at 101.5 10.0 ft. long. This assumes boards removed to crest; lst from side spillways, then from end.

Elev.	•0	•1	•2	•3	•4	•5	•6	•7	•8	•9
101						•0	•0	•1	•2	•3
2	•4	-4	•5	•5	•6	• 7	•7	.8 1.5	•9	1.0
3	1.1	1.1	1.2	1.3	1.3	1.4	1.4	1.5	1.6	1.7
Ĭ.	1.8	1.8	1.9	1.9	2.0	2.1	2.1	2.2	2.3	2.4
<b>1</b> 05	2.5	2.5	2.6	2.7	2.8	2.9	2.9	3.0	3.0	3.1
6	3.2	3.2	3.3	3.4	3.5	3.6	3.6	3.7	3.7	3.8
7	3.9	3.9	4.0	4.1	4.2	4.3	4.3	4.4	4.4	4.5
8	4.6	4.6	4.7	4.8	4.9	5.0	5.0	5.1	5.2	5.3
9	5.4	5.4	5.5	5.5	5.6	5.7	5.7	5.8	5•2 5•9	6.0
110	6.1	6.1	6.2	6.2	6.3	6.4	6.4	6.5	6.5	6.6
11	6.7	6.8	6.9	7.0	7.1	7.2	7.2	7.3	7.3	7.4
12	7.5	•-	•	, •	. •					

All Spillways, over top of boards, 46.4 ft. long.

11aad a		p							-	
Head on boards	•0»·	•1	•2	•3	•4	•5	•6	•7	.8	•9
0 1	.0 3.4	.1 3.9	•3 4•4	•5 4•9	•8 5•5	1.2 6.0	1.6 6.6	2.0 7.2	2•4 7•8	2.9 8.4
2	9.0 16.0	9•7	10.3	11.0	11.7	12.3	13.1	13.8	14.5	15.3

Note: These values reflect effect of backwater of Discharge Waterway. Also interference of side and end spillways.

D-8

N.E.P.S.Co. 9-1-1953 G.N.B.

#### PROJECT = (1-1-1/4)

DATE - The state of the state o COMPUTED BY \_\_\_\_\_\_\_\_\_.

BUBBERT RESIDES STORES FOR STANERSED FLOODING - 10/x15/ FILL JELLERS.

A = 10 x15 = 150.0 000 1/1/2.

Q = Cx · A. J264 = 0.45 × 150 × 8. 15

= 5-40 x (9

ELEVATION

89.0

91.0

93.0

95.0

9.7 1.0

99.0 . . .

101.0

103.0- 14.5 103 . 5 . . . 15.0

104.0 15-15

105-10

16.5

106.0 17.5 18.5

. 107. D. . 108.0

19.5

109.3 20.5 110.0 21.5

111.0 22.5

:- 23,5 112.0

94

1687.0

1988 0 2091 0

2126,0

2193.0

2259.0

2323.0

2385.0

2445.0 25.0410

2561.0

2618.0

#### PROJECT <u>EN-006 (4)</u>

FILE NUMBER EIJ-005 BHEET NUMBER 10

DATE 8-29-73

OUBJECT COMPOSITE PATING CURVE

COMPUTED BY 2/1/1

GDD'S POND DAM

ELEVATION	Q=Q1+Q2+Q3+Q4
83.0	0,
85.0	64.0
87.0	168.0
89.0	248.0
91.0	320.0
93.0	384.0
95.0	440.0
97.0	496.0
99.0	552.0
101.0	600.0
101.5	2,295.0
103.0	2,849.0
104.0	3,211.0
105.0	3,696.0
106.0	3,886.0
107.0	4,275.0
103.0	4,695.0
109.0	5,153.0
110.0	5,625.0
11110	5,928.0
112.0	6,641.0

#### GRANITE STATE ELECTRIC COMPANY GOOSE POND STORAGE DATA

D.A. 15.7 Sq. Mi.

10 Feet at 19.5 Crest G. H. 36'-5" at 16.5 Minimum Drawdown G.H. 0.0

G.H. Feet		Area Acres	Acre Feet		f.s. ays	Inche 15.7 S		M.C.F	•	Thous. KWH $K = 4.6$
0		376	0		0		0	0		0
ī		1.00	388		195	•	464	16.9		21.6
2		424	800		403	٠, •	955	34.8		5 بلبل
1.		1445 1461	1234 1689		622 852	1.	474 017	53.8 73.6		68.7 94.0
3 45/6		480	2161		090	2.	581	94.1		120.3
چ		495	2648		355	3.	163	115.3		147.4
7 8		508	3150	1	588	3.	762	137.2		175.3
8		521	3665		848	<b>4.</b>	376	159.6	ı	204.0
9		532	<u>h</u> 191		114	5.	006	182.6		233.3
10		543	4730		385	<u> </u>	678	206.0		263.3
11 12		554 565	5279 5838	2	662	6.	304	229.9		293.8
13		505 575	6408		943 231	7	973 653	254.3 279.1		324.9 356.7
14		585	6988	, 1	524	8.	346	304.4		389.0
<u> </u>		596	7579		821		05?	330.2		421.8
16		607	8181		125		771	356.4		455.4
17		618	8794	4	434	10.	503	383.1		489.5
18		629	9418	հ	748	11.	5118	410.3		524.2
19_		640	10053		069	12.		437.9		559.5
20		652	10599		39 <u>5</u>	12.	778	466.1		595.5 632.i.
21 21.	5	663 668	11356 11688	5	726 <b>89</b> 3	13. 13.	959	494.6 509.1		650.6
					C.F.S.	DAYS				
G.H.	0	.1	•2	•3	•4	•5	.6	•7	.8	•9
0	0	19	38	5?_	76	95	115_	135 539	155	175
ī	195	215	235	255	275	296	317	539	360	382
2	403	H2H	1116	և67	489	510	532	555	578	600
3	622	645	668	690	71.2	735	758	782	805 1012	829 1066
3 4 5 6	852 1090	875 111!:	899 1138	922 1163	946 1187	959 1211	993 1235	1017 1261	1286	1311
<del>}_</del> _	1335	1360	1385	1410	1435	1460	1486	1511	1537	1562
7	1588	1614	1639	1665	1690	1716	1742	1769	1795	1821
8	1848	1874	1900	1926	1953	1979	2006	2033	2060	2087
9	2114	2140	2167	2194	2221	5578	2275	2303	2330	2358
10	2385	շև12	2l14C	2467	2495	2522	2550	2578	2606	26 <u>3</u> 4
11	2662	2689	2717	2745	2773	2801.	2829	2858	2887	2915
12	2943	2972	3000	3028	3057	3086	3115	3144	3173	3202
13	3231	3260	3289 3583	3318	3347 3642	3376	3406 3203	3435 3731	3465 3761	كارىلا 3791
池	352l <sub>4</sub> 3821	3553 3852	3582 3882	3612 3912	391,2	3671 3972	3701. 4003	4033	406L	1001
15 16	1125	4156	4186	1217	4247	4278	4309	4340	4372	1403
17	4434	44.65	7786	1528	4559	4590	4622	4653	4685	4717
ī8	4748	4780	4812	4844	4875	4907	4939	4972	5007	5037
19	5069	5101	5134	51.66	5199	5231	5254	5297	5329	5362
20	5395	5428	546.1	5493	5526	5559	5592	5626	5659	5693
21	5726	5759	5793	5826	5860	5893				

N.E.P.S.Co. L.D. Pierce 3-28-61

FILE NUMBER French PROJECT <u>EN-006 (4)</u> SHEET NUMBER / --BUBJECT GOOSE POND DAM COMPUTED BY 5 STORAGE APOUF FLEV 1015 STORAGE ABOUT STORAGE MOON ELEV 101.5 TOTAL STORAGE EVEV. 101.5 ACRE-FEET). Fr3 ELEVATION ACRE-FEET . ....8487 0 101.5 13.34 ×106 .....8794 307 102,0 40,55×10 931 9418 103.0 1566 68,21×10 10053 104.0 96-35X106 10699 2212 105.0. 124,978166 2869 1.1356 106.0 139.44×10 320/ 106.5 11688 REFER TO THBLE ON PAGE 11

OUDJECT GOVER POND THIN

STIP BY STEP THINK PAIN YE CHICALATHONS

377																					
STEURTION STEER		101.4	161.4	101.4	10/5	101.8	102.3	102.9	103.5	1041	104.6	1049	1/50/	165.2	105.3	105.3	105.3	165.3	705.2	163.3	105,2
RESERVAN LEVEL		101.4	4101	101.9	1015	101.7	102.3	102.9	103.5	164.1	13.7.6	104.9	165.1	160.2	125.3	105.3	165.3	8 901	105.3	5201	~) ~) ~)
STORMSE BY THE ENO OF CHENCEL		7.08x10	1.5346	1.17 1106	1.86x169 70.72×164	1 801/106	18.90×m5	35,35,40	53,4CK10	76.37×10	83,94×10°	93.7.186	38864116	337×16 102,017.06	216516 169,11X16	133416 105 Sone	6.618 10011 16.	0.00x36 10609106	105,4286	104.59ro	163.4X65
STORAGE IN THE OLDS A STORAGE		1		10,361/6 1.17 X106		79185.7	37X01781	16.43466	92/K/181	12811871	13,571 116	923×106	5.47×16	33716				6. Cax 36	C1.1716	2.63x10 -0.83x16 104.5916	2,63x16 -1,19x16 163,4x16:
STORNGE	00	1.35×106	1.26×106	1.26 1/06	1.35 ×106	201251	,0X2C1	1.41×106	2.05 1/6	30X/CZ	3.36 110°	2,47×106	2.541106	2,57766	2.611166	3.63×106	2,63×16	2,63.11	2 63405-	2.63x6	3.KEJ.C
OUTTOW OS CEND OF JATTOWY	7	1750	1750	1200	2000	2350	2550	2750	2950	3700	3350	2560	3550	3600	3650	3650	3650	3650	2650	3650	3650
INFIGO OUTFLOU STORAGE O, I, HI, T (BEGINNING A) SHERMILL  ET3 (ES	e	7000	1750	1750	1750	2000	2350	0552	2750	2950	3200	3350	3560	3550	3600	2650	3650	3656	3650	3650	3650
	ķη	0.27.8106	90/x/30	162 × 10 6	3.2.7x166	7,657,106	1286×106	1836x106	20/6xise	0 19.12×166	, 9/x2651 C	15,000 11.704106	1,430, 201166	C 5.99 1.10°	4.77 x/6°	3.76.116	374 10	777 1195	612.16x106	18x6°	1,44x1051
INFLOW  I.A. (END OF  SAMPHUML)  (F.S.	7	750	1,500	3,000	0007	15,250	23,250	27,750	28,250 Lalexist	24,750	11,500	13,000	9,430	U7:2%	00009	5,000	0	0		2,250	1,750
INFLOWD  I  (BEGINNING  OF INTERNIT	~)	٥	750	1,500	2,000	0009	-	03250		28,250	24750	19,500	13,000	1,250	1,550	0000	5,000	600	27.50	3750	2,256
TIME INTERVAL	~	2.0-0.2	4.0.80	0.4-0.6	80-95	0.8-1.0	1.0-12	1.3-14	1.1-1.6	16-1.8	1.9-20	6.6-0.C	3.3.3.4	978-46	3.6-2.6	28 30	20.02	12.24	`` `` ```	3,673,8	200
C 24		~	~	۲)	4	6	e	~	<i>O</i>	/5	0/	1	12		1	.5	9,	1.1	ă.	5	ر ان

#### PROJECT #11-001 (11)

FILE NUMBER EN- 01

BHEET NUMBER 114

DATE 7-20-1978

SUBJECT GOORE POND DIAM.

ESTIMETION OF DEPTH OF FLU DWATE CHECKED BY

IN THE VICINITY OF DAMAGE IMPACT AREA DUE TO BREACH IN THE DAM AT RECENCIE.

Ad emploined in dection 12 d, it is not possed to

to generate downstrusion dam Januar hydrograph in the midnity of the some general and impact area, using USGS quadrang a sheet on which the contours are at 20-foot untowards.

was a vailable for the area.

impact area and the course of the damage and bull park which made has been made as follows:

Dipth of Water above the Kinerled at F.R.L

= 106.5-81.5

= 25.0

Hught of Herd wave at damage impact

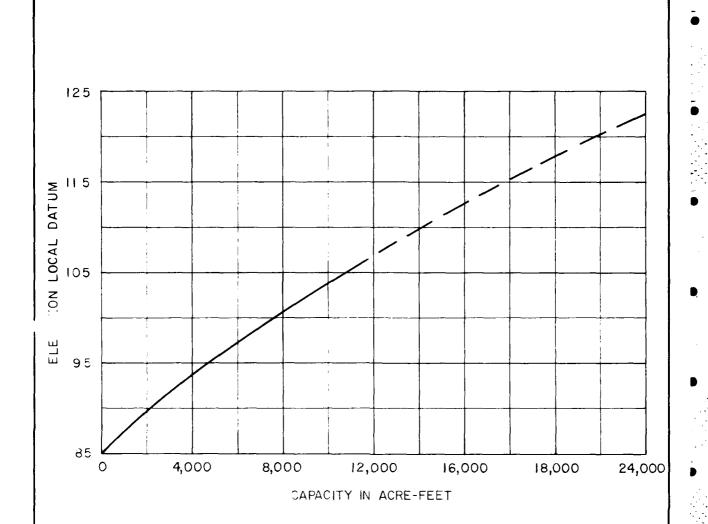
area is estimated to be 15 feet.
Midth of water spread at damage impact
area is approximately indicated on the
USGS MAP included in the APPENDIX-D.

FAY, SPOFF OND A THORNIDIKE, INC.

U.S. PRINT ENGINEERS
ENGINEERS
ENGINEERS
ENGINEERS
ENGINEERS

WALTHAM, MASS

NATIONAL PROGRAM OF INSPECTION OF NON-FED. DAMS GOOSE POND DAM SPILLWAY TEST FLOOD INFLOW HYDROGRAPH



STORAGE CAPACITY - ELEVATION CURVE

106.5 (LOCAL DATUM) = 825 USGS (ESTIMATED)

FAY, SPOFFORD & THORNDIKE, INC.
ENGINEERS
BOSTON, MASS.

U.S. ARMY ENGINEER DIV. NEW ENGLAND
CORPS OF ENGINEERS
WALTHAM, MASS.

NATIONAL PROGRAM OF INSPECTION OF NON-FED DAMS

#### GOOSE POND DAM

GOOSE POND BROOK

SCALE AS SHOWN
DATE AUGUST, 1978

୦୦୯'୦। 000'6 000'8 2,000 RATING CURVE (COMPOSITE) FOR SPILLWAY AND DAM 6,000,0 COMPOSITE DISCHARGE IN CES

FAY, SPOFFORD BTHORNOIKE, INC. ILLS ARMY ENGINEER DIV NEW ENGLAND ENGINEERS.

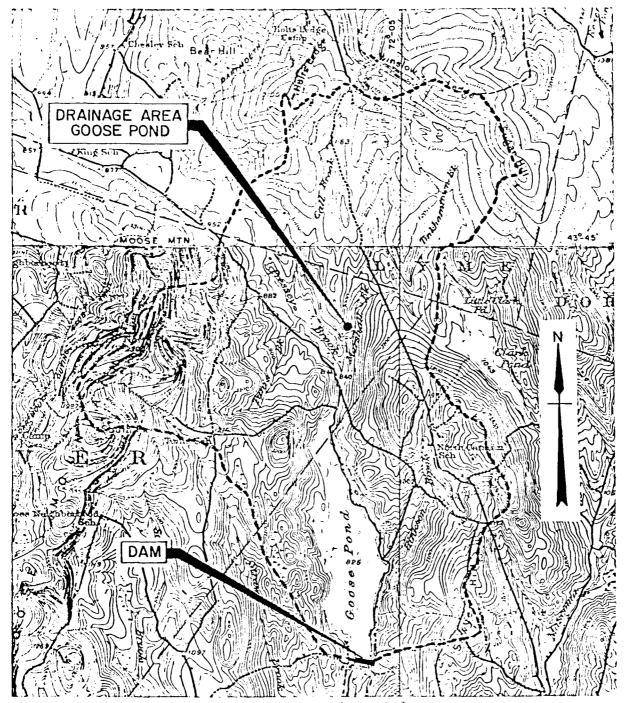
BOSTON, MASS. "HALTHAM, MASS.

NATIONAL PROGRAM OF INSPECTION OF NON-FED DAMS

GOOSE POND DAM

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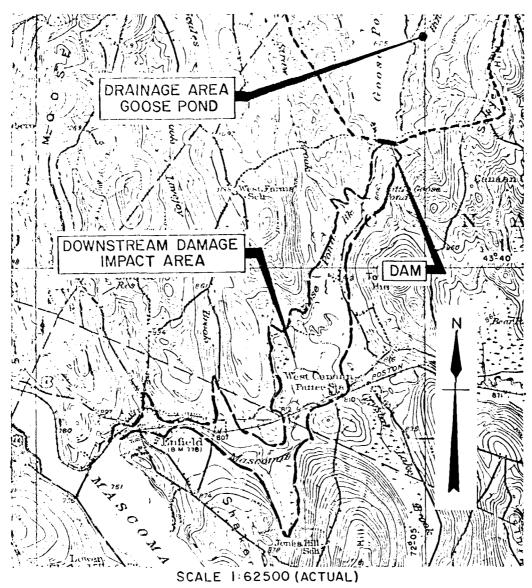
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SCALE : 1:62500 (ACTUAL)

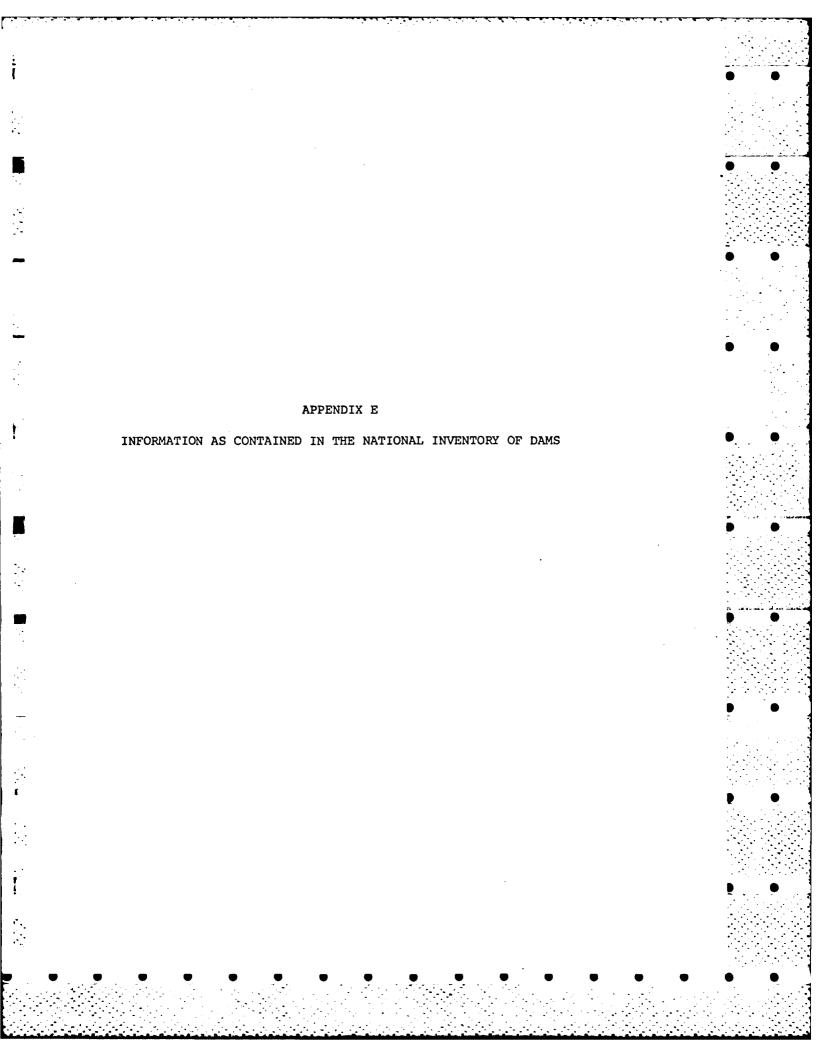
UNITED STATES
DEPARTMENT OF INTERIOR
GEOLOGICAL SURVEY

NEW HAMPSHIRE-VERMONT MASCOMA QUADRANGLE 1927 MT. CUBE QUADRANGLE 1931



UNITED STATES
DEPARTMENT OF INTERIOR
GEOLOGICAL SURVEY

NEW HAMPSHIRE-VERMONT MASCOMA QUADRANGLE 1927



# INVENTORY OF DAMS IN THE UNITED STATES

TATILITY LOYGING RIPORT BALE	17295.5	NAME OF INVOINIONENT	(1)  (1)  (1)  (1)  (1)  (2)  (1)  (2)  (3)  (4)  (4)  (5)  (6)  (7)  (7)  (7)  (7)  (8)  (9)  (1)  (1)  (1)  (1)  (1)  (2)  (3)  (4)  (4)  (4)  (5)  (5)  (6)  (7)  (7)  (7)  (7)  (8)  (9)  (9)  (1)  (1)  (1)  (1)  (1)  (2)  (1)  (2)  (3)  (4)  (4)  (4)  (5)  (6)  (7)  (7)  (7)  (7)  (8)  (9)  (9)  (9)  (9)  (9)  (9)  (9	098	MONTHING CAPACITIES  MONTHING CAPACITIES  MONTHING CAPACITIES  OF IN FLO H PHYZFED SCS	15800 11700 NED N N N N		ANACHY (i) (i) (ii) (ii) (ii) (ii) (ii) (ii)	(5)	CONSTRUCTION BY	13 H B	PERATION	NH WATER WES BD TH AATEM ALS BD	AHTHOPHY	PL92-367	
ALLIAN TRUESTES, STATE COUNTY, MAN JAME COUNTY AND THE COUNTY AND	SALORY CEL	POITULAR NAME	The continue of the continue o	COURT ANDORA	(a) (b) (c) (b) (c) (c) (d) (d) (d) (d) (d) (d) (d) (d) (d) (d	recire 1718 KS 31 20	nemanks	11 STREET WAY (9) (9) (9) (9) (9) (9) (9) (9) (9) (9)	1 1 1 2 0 0 5 0 0 5 0 0 5 0 0 0 0 0 0 0 0 0 0	OWILCA	STATE OF MEW HAMPSHIPE NASCOMA HIVER INPR CO	10 COBS	10 NH WATER RES BD	HASPE	IORUDIKE, INC.	

## END

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